Made available by Hasselt University Library in https://documentserver.uhasselt.be

On asymptotic normality in estimation after a group sequential trial Peer-reviewed author version

BERCKMOES, Ben; IVANOVA, Anna & MOLENBERGHS, Geert (2020) On asymptotic normality in estimation after a group sequential trial. In: Sequential analysis, 39 (4), p. 443 -466.

DOI: 10.1080/07474946.2020.1826784 Handle: http://hdl.handle.net/1942/33469

On Asymptotic Normality in Estimation after a Group Sequential Trial

Ben Berckmoes*, Anna Ivanova**, Geert Molenberghs**

*Department of Mathematics, University of Antwerp, Antwerp, Belgium **CenStat, University of Hasselt, Hasselt, Belgium **L-BioStat, University of Leuven, Leuven, Belgium

Abstract: We prove that in many realistic cases, the ordinary sample mean after a group sequential trial is asymptotically normal if the maximal number of observations increases. We derive that it is often safe to use naive confidence intervals for the mean of the collected observations, based on the ordinary sample mean. Our theoretical findings are confirmed by a simulation study.

Keywords: Asymptotic normality; Confidence interval; Group sequential trial; Sample mean

Subject Classifications: 62L12

1. INTRODUCTION

Throughout this paper, we will tacitly assume that all random variables are defined on the same probability space. Furthermore, we will keep fixed

- parameters $\mu \in \mathbb{R}$ and $\sigma \in \mathbb{R}_0^+$,
- a sequence X_1, X_2, \ldots of i.i.d. random variables with normal law $N(\mu, \sigma^2)$,
- a natural number $L \in \mathbb{N}_0$,
- natural numbers $0 < k_1 < k_2 < ... < k_{L+1}$,
- a Borel measurable map $\psi: \mathbb{R} \to [0, 1]$,
- a parameter $\gamma \in \mathbb{R}^+$.

Also, for each $n \in \mathbb{N}_0$, we will keep fixed a random sample size N_n such that

- N_n can take the values $k_1 n, \ldots, k_{L+1} n$,
- for each $i \in \{1, \dots, L\}$, the event $\{N_n = k_i n\}$ does not depend on $X_{k_i n+1}, X_{k_i n+2}, \dots$,
- for each $i \in \{1, \dots, L\}$, the stopping rule

$$\mathbb{P}[N_n = k_i n \mid X_1, \dots, X_{k_i n}] = \psi \left(K_{k_i n} / (k_i n)^{\gamma} \right) \prod_{i=1}^{i-1} (1 - \psi) \left(K_{k_j n} / (k_j n)^{\gamma} \right)$$
(1.1)

holds, where, for $m \in \mathbb{N}_0$, $K_m = \sum_{k=1}^m X_k$, and the empty product is 1.

For each $n \in \mathbb{N}_0$, the above mathematical model represents a group sequential trial in which the observations X_1, X_2, \ldots are collected, and which has random length N_n . After having collected the observations $X_1, \ldots, X_{k_1 n}$, an interim analysis of the sum $K_{k_1 n} = \sum_{k=1}^{k_1 n} X_k$ is performed, and, based on the stopping rule (1.1) with i=1, one decides whether the trial is stopped, i.e. has length $k_1 n$, or continued, i.e. the additional observations $X_{k_1 n+1}, \ldots, X_{k_2 n}$ are collected, and a new interim analysis of the sum

Address correspondence to B. Berckmoes, Department of Mathematics, University of Antwerp, Antwerp, Belgium; E-mail: ben.berckmoes@uantwerpen.be

 $K_{k_2n} = \sum_{k=1}^{k_2n} X_k$ is performed, based on the stopping rule (1.1) with i=2. This process continues either until the trial is stopped at a point where an interim analysis is performed, or until the maximal length $k_{L+1}n$ is reached. Thus the actual length N_n can take the values $k_1n, k_2n, \ldots, k_{L+1}n$.

We wish to point out that the above mathematical model contains a very popular setting in sequential analysis. Indeed, if we let

- for each $i \in \{1, ..., L+1\}, k_i = i$,
- ψ be the map

$$\psi(x) = \begin{cases} 1 & \text{if} \quad |x| \ge C \\ 0 & \text{if} \quad |x| < C \end{cases}, \tag{1.2}$$

where $C \in \mathbb{R}_0^+$ is a fixed constant,

then N_n becomes a random sample size such that

- N_n can take the values $n, 2n, \ldots, (L+1)n$,
- for each $i \in \{1, \dots, L\}$, the event $\{N_n = in\}$ does not depend on $X_{in+1}, X_{in+2}, \dots$,
- for each $i \in \{1, \dots, L\}$, the stopping rule (1.1) is transformed into

$$\mathbb{P}[N_n = in \mid X_1, \dots, X_{in}]$$

$$= \begin{cases} 1 & \text{if} \quad |K_{in}| \ge C(in)^{\gamma} \text{ and } \forall j \in \{1, \dots, i-1\} : |K_{jn}| < C(jn)^{\gamma} \\ 0 & \text{otherwise} \end{cases}$$

$$(1.3)$$

So this situation corresponds to a group sequential trial in which independent observations with law $N(\mu, \sigma^2)$ are collected, and in which an interim analysis of the sum of the observations is performed after every n observations. The stopping rule (1.3) indicates that the trial is stopped either at the first in for which $|K_{in}|$ exceeds $C(in)^{\gamma}$, or at (L+1)n. This example has been studied extensively in the literature, see e.g., Siegmund (1978), Chang (1989), and Woodroofe (1992). The number γ is called the shape parameter. The choice $\gamma = 1/2$ is known as the Pocock paradigm, introduced in Pocock (1977), and the choice $\gamma = 0$ as the O'Brien-Fleming paradigm, introduced in O'Brien et al. (1979).

We now return to the general setting, determined by the first two paragraphs of this section. We are interested in the asymptotic behavior of the sample mean $\widehat{\mu}_{N_n} = K_{N_n}/N_n$, used as an estimator for μ , as $n \to \infty$. Notice that, L and the k_i being kept fixed, we are in fact looking at the asymptotics of a group sequential trial in which the maximal sample size $k_{L+1}n$ increases, but in which the number L of interim analyses is fixed, and in which, for each $i \in \{1, \dots, L\}$, the ratio of the number of observations collected at the ith interim analysis, i.e. $k_i n$, to the maximal number of observations, i.e. $k_{L+1}n$, is a fixed number, i.e. k_i/k_{L+1} .

Very recently, building upon Molenberghs et al. (2014), the bias and the mean squared error (MSE) of the sample mean $\hat{\mu}_{N_n}$ were studied in Berckmoes et al. (2018). From the general results obtained in that paper, it can be easily derived that $\hat{\mu}_{N_n}$ is asymptotically unbiased in the sense that

$$\mathbb{E}\left[\widehat{\mu}_{N_n} - \mu\right] \to 0 \text{ as } n \to \infty \text{ with rate } 1/\sqrt{n},$$

and has a vanishing MSE in the sense that

$$\mathbb{E}\left[\left(\widehat{\mu}_{N_n}-\mu\right)^2\right]\to 0 \text{ as } n\to\infty \text{ with rate } 1/n.$$

Moreover, the rates $1/\sqrt{n}$ and 1/n were shown to be optimal.

Concerning asymptotic normality of $\widehat{\mu}_{N_n}$, first steps were taken in Berckmoes et al. (2018), but the authors were not able to prove a powerful result. In this paper, building upon Berckmoes et al. (2018), we will prove an asymptotic normality result for $\widehat{\mu}_{N_n}$ in the general setting.

The paper is structured as follows. In section 2, we formulate some preliminary results from Berckmoes et al. (2018). In section 3, a fundamental equation will be derived from the theory developed in Berckmoes et al. (2018). In section 4, we provide the main result of this paper, which states that the quantity $\frac{\sqrt{N_n}}{\sigma} (\widehat{\mu}_{N_n} - \mu)$ converges to N(0,1) for the total variation distance as $n \to \infty$ in each of the following cases:

- (A) $\gamma > 1$ and ψ has a finite limit in 0,
- (B) $\gamma = 1$ and ψ has a finite limit in μ ,
- (C) (1) $1/2 < \gamma < 1$, $\mu \neq 0$, and ψ has finite limits in $-\infty$ and ∞ ,
 - (2) $1/2 < \gamma < 1$, $\mu = 0$, and ψ has a finite limit in 0,
- (D) $\gamma = 1/2, \mu \neq 0$, and ψ has finite limits in $-\infty$ and ∞ ,
- (E) (1) $0 < \gamma < 1/2$, $\mu \neq 0$, and ψ has finite limits in $-\infty$ and ∞ ,
 - (2) $0 \le \gamma < 1/2$, $\mu = 0$, and ψ has coinciding finite limits in $-\infty$ and ∞ .

Notice that the conditions imposed on ψ are mild, and are always satisfied if ψ takes the form (1.2) and $\mu \notin \{-C, C\}$. The proof of the main result is based on the fundamental equation formulated in section 3. We also state a conclusion for the validity of confidence intervals for the parameter μ based on $\widehat{\mu}_{N_n}$. In section 5, some examples are given, which show that the conditions under which the main result holds, cannot be omitted. A simulation study is conducted in section 6. Some concluding remarks are formulated in section 7.

2. PRELIMINARIES

Let ϕ be the standard normal density. For a finite tuple $B=(b_1,\ldots,b_i)$ of bounded Borel measurable maps of $\mathbb R$ into $\mathbb R$, the *normal transform* was defined in Berckmoes et al. (2018) (section 2, first paragraph) as the map $\mathcal N_{B,\mu,\sigma}$ of $]0,\infty[^{i+1}\times\mathbb R]$ into $\mathbb R$ given by

$$\mathcal{N}_{B,\mu,\sigma}(x_1, \dots, x_{i+1}, x) = \frac{\int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} \prod_{j=1}^{i} \frac{\phi\left(\frac{z_j - \mu x_j}{\sigma\sqrt{x_j}}\right)}{\sigma\sqrt{x_j}} b_j\left(\sum_{k=1}^{j} z_k\right) \frac{\phi\left(\frac{x - \sum_{k=1}^{i} z_k - \mu x_{i+1}}{\sigma\sqrt{x_{i+1}}}\right)}{\sigma\sqrt{x_{i+1}}} dz_i \dots dz_1}{\frac{1}{\sigma\sqrt{\sum_{k=1}^{i+1} x_k}} \phi\left(\frac{x - \mu\sum_{k=1}^{i+1} x_k}{\sigma\sqrt{\sum_{k=1}^{i+1} x_k}}\right)}$$

The following recursive description of the normal transform was obtained in Berckmoes et al. (2018) (section 2, Theorem 3).

Theorem 2.1. Let ξ be a random variable with law N(0,1). For a bounded Borel measurable map b of \mathbb{R} into \mathbb{R} , $x_1, x_2 \in]0, \infty[$, and $x \in \mathbb{R}$,

$$\mathcal{N}_{b,\mu,\sigma}(x_1, x_2, x) = \mathbb{E}\left[b\left(\frac{x_1}{x_1 + x_2}x + \sigma\sqrt{\frac{x_1 x_2}{x_1 + x_2}}\xi\right)\right]. \tag{2.1}$$

Furthermore, for a natural number $i \geq 2$, a tuple (b_1, \ldots, b_i) of bounded Borel measurable maps of \mathbb{R} into \mathbb{R} , $x_1, \ldots, x_{i+1} \in]0, \infty[$, and $x \in \mathbb{R}$,

$$\mathcal{N}_{(b_1,\dots,b_i),\mu,\sigma}(x_1,\dots,x_{i+1},x) = \mathcal{N}_{(b_1,\dots,b_{i-2},\tilde{b}_{i-1}),\mu,\sigma}(x_1,\dots,x_{i-1},x_i+x_{i+1},x), \tag{2.2}$$

where

$$\widetilde{b}_{i-1}(z) = b_{i-1}(z) \mathbb{E}\left[b_i \left(\frac{x_{i+1}}{x_i + x_{i+1}}z + \frac{x_i}{x_i + x_{i+1}}x + \sigma\sqrt{\frac{x_i x_{i+1}}{x_i + x_{i+1}}}\xi\right)\right]. \tag{2.3}$$

For all $n \in \mathbb{N}_0$ and $i \in \{1, \dots, L\}$, put

$$m_{n,i} = k_i n, (2.4)$$

and

$$M_n = k_{L+1}n. (2.5)$$

Also, for all $n \in \mathbb{N}_0$ and $i \in \{1, \dots, L\}$, let $\psi_{m_{n,i}}$ be the Borel measurable map defined by

$$\psi_{m_{n,i}}(x) = \psi(x/m_{n,i}^{\gamma}). \tag{2.6}$$

Then, by the second paragraph of section 1, N_n is a random sample size such that

- N_n can take the values $m_{n,1}, \ldots, m_{n,L}, M_n$,
- for each $i \in \{1, \dots, L\}$, the event $\{N_n = m_{n,i}\}$ does not depend on $X_{m_{n,i}+1}, X_{m_{n,i}+2}, \dots$,
- for each $i \in \{1, \dots, L\}$, the stopping rule

$$\mathbb{P}[N_n = m_{n,i} \mid X_1, \dots, X_{m_{n,i}}] = \psi_{m_{n,i}} \left(K_{m_{n,i}} \right) \prod_{j=1}^{i-1} (1 - \psi_{m_{n,j}}) \left(K_{m_{n,j}} \right)$$

holds.

This brings us exactly in the setting of Berckmoes et al. (2018) (section 1, first paragraph). Now, as in Berckmoes et al. (2018) (section 3, first paragraph), put

$$\Delta m_{n,1} = m_{n,1} \tag{2.7}$$

and

$$\mathcal{N}_{n,1}(x) = 1, (2.8)$$

and, for $i \in \{2, ..., L\}$,

$$\Delta_{m_{n,i}} = m_{n,i} - m_{n,i-1} \tag{2.9}$$

and

$$\mathcal{N}_{n,i}(x) = \mathcal{N}_{(1-\psi_{m_{n,1}},\dots,1-\psi_{m_{n,i-1}}),\mu,\sigma}(\Delta_{m_{n,1}},\dots,\Delta_{m_{n,i}},x).$$
(2.10)

The following result was obtained in Berckmoes et al. (2018) (section 7, Lemma 17).

Theorem 2.2. Let ξ and η be independent random variables with law N(0,1). Then, for each $n \in \mathbb{N}_0$ and each bounded Borel measurable test function $h : \mathbb{R} \to \mathbb{R}$,

$$\mathbb{E}\left[\left\{h(\xi) - h\left(\frac{\sqrt{N_n}}{\sigma}\left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right] = \sum_{i=1}^{L} \mathbb{E}\left[h(\xi)\left\{\mathcal{M}_i(n) - \widetilde{\mathcal{M}}_i(n)\right\}\right],\tag{2.11}$$

with

$$\mathcal{M}_i(n) = \left(\psi_{m_{n,i}} \mathcal{N}_{n,i}\right) \left(\mu m_{n,i} + \sigma \sqrt{m_{n,i}} \xi\right)$$

and

$$\widetilde{\mathcal{M}}_i(n) = \left(\psi_{m_{n,i}} \mathcal{N}_{n,i}\right) \left(\mu m_{n,i} + \sigma \sqrt{\frac{m_{n,i}(M_n - m_{n,i})}{M_n}} \xi + \sigma \frac{m_{n,i}}{\sqrt{M_n}} \eta\right).$$

In the next section of this paper, we will combine the recursive description of the normal transform in Theorem 2.1 with equation (2.11) in Theorem 2.2, to obtain a fundamental equation.

3. A FUNDAMENTAL EQUATION

We will state a fundamental equation in Theorem 3.1. We first need two lemmas.

Lemma 3.1. For each $i \in \{2, ..., L\}$, the following assertion holds. For each collection of real numbers $0 < x_1 < x_2 < ... < x_i$, there exist fixed continuous random variables $\rho_{i,1}, \rho_{i,2}, ..., \rho_{i,i-1}$, only depending on σ and the x_j , such that, for each $n \in \mathbb{N}_0$, each collection $b_1, ..., b_{i-1}$ of bounded Borel measurable maps of \mathbb{R} into \mathbb{R} , and each $x \in \mathbb{R}$,

$$\mathcal{N}_{(b_1,\dots,b_{i-1}),\mu,\sigma}(x_1n,x_2n,\dots,x_in,x) = \mathbb{E}\left[\prod_{j=1}^{i-1} b_j \left(\frac{\sum_{k=1}^j x_k}{\sum_{k=1}^i x_k} x + \rho_{i,j}\sqrt{n}\right)\right].$$
(3.1)

Proof. Assume that $L \geq 2$. The proof is by induction on $i \in \{2, \dots, L\}$, using Theorem 2.1.

Take i=2, strictly positive real numbers $x_1, x_2, n \in \mathbb{N}_0$, a bounded Borel measurable map b of \mathbb{R} into \mathbb{R} , and $x \in \mathbb{R}$. Fix a standard normally distributed random variable ξ . Then, by (2.1),

$$\mathcal{N}_{b_1,\mu,\sigma}(x_1 n, x_2 n, x) = \mathbb{E}\left[b_1\left(\frac{x_1}{x_1 + x_2}x + \sigma\sqrt{\frac{x_1 x_2}{x_1 + x_2}}\xi\sqrt{n}\right)\right].$$

Thus, putting

$$\rho_{2,1} = \sigma \sqrt{\frac{x_1 x_2}{x_1 + x_2}} \xi,$$

shows that the desired assertion holds for i = 2.

Now assume that L > 2 and that the desired assertion holds for some $i \in \{2, \ldots, L-1\}$. We will prove that it also holds for i+1. Take strictly positive real numbers $x_1, x_2, \ldots, x_{i+1}, n \in \mathbb{N}_0$, bounded Borel measurable maps b_1, \ldots, b_i of \mathbb{R} into \mathbb{R} , and $x \in \mathbb{R}$. By (2.2) and (2.3),

$$\mathcal{N}_{(b_1,\dots,b_i),\mu,\sigma}(x_1n,\dots,x_{i+1}n,x) = \mathcal{N}_{(b_1,\dots,b_{i-2},\tilde{b}_{i-1}),\mu,\sigma}(x_1n,\dots,x_{i-1}n,(x_i+x_{i+1})n,x),$$
(3.2)

where, for any standard normally distributed random variable ξ ,

$$\widetilde{b}_{i-1}(z) = b_{i-1}(z) \mathbb{E}\left[b_i \left(\frac{x_{i+1}}{x_i + x_{i+1}}z + \frac{x_i}{x_i + x_{i+1}}x + \sigma\sqrt{\frac{x_i x_{i+1}}{x_i + x_{i+1}}}\xi\sqrt{n}\right)\right]. \tag{3.3}$$

By the induction hypothesis applied to $x_1, \ldots, x_{i-1}, x_i + x_{i+1}$, there exist fixed continuous random variables $\rho_{i,1}, \ldots, \rho_{i,i-1}$, only depending on σ and the x_i , such that

$$\mathcal{N}_{(b_{1},\dots,b_{i-2},\widetilde{b}_{i-1}),\mu,\sigma}(x_{1}n,\dots,x_{i-1}n,(x_{i}+x_{i+1})n,x)
= \mathbb{E}\left[\prod_{j=1}^{i-2}b_{j}\left(\frac{\sum_{k=1}^{j}x_{k}}{\sum_{k=1}^{i+1}x_{k}}x+\rho_{i,j}\sqrt{n}\right)\widetilde{b}_{i-1}\left(\frac{\sum_{k=1}^{i-1}x_{k}}{\sum_{k=1}^{i+1}x_{k}}x+\rho_{i,i-1}\sqrt{n}\right)\right].$$
(3.4)

But then, fixing a standard normally distributed random variable ξ , stochastically independent of $\rho_{i,1},\ldots,\rho_{i,i-1}$,

and combining (3.2), (3.3) and (3.4), gives

$$\mathcal{N}_{(b_{1},\dots,b_{i}),\mu,\sigma}(x_{1}n,\dots,x_{i+1}n,x) \\
= \mathbb{E}\left[\prod_{j=1}^{i-1}b_{j}\left(\frac{\sum_{k=1}^{j}x_{k}}{\sum_{k=1}^{i+1}x_{k}}x + \rho_{i,j}\sqrt{n}\right)\right] \\
b_{i}\left(\frac{x_{i+1}}{x_{i}+x_{i+1}}\left(\frac{\sum_{k=1}^{i-1}x_{k}}{\sum_{k=1}^{i+1}x_{k}}x + \rho_{i,i-1}\sqrt{n}\right) + \frac{x_{i}}{x_{i}+x_{i+1}}x + \sigma\sqrt{\frac{x_{i}x_{i+1}}{x_{i}+x_{i+1}}}\xi\sqrt{n}\right)\right] \\
= \mathbb{E}\left[\prod_{j=1}^{i-1}b_{j}\left(\frac{\sum_{k=1}^{j}x_{k}}{\sum_{k=1}^{i+1}x_{k}}x + \rho_{i,j}\sqrt{n}\right)\right] \\
b_{i}\left(\frac{\sum_{k=1}^{i}x_{i}}{\sum_{k=1}^{i+1}x_{k}}x + \left(\frac{x_{i+1}}{x_{i}+x_{i+1}}\rho_{i,i-1} + \sigma\sqrt{\frac{x_{i}x_{i+1}}{x_{i}+x_{i+1}}}\xi\right)\sqrt{n}\right)\right].$$

Thus, considering the collection of continuous random variables $\tilde{\rho}_{i+1,1},\ldots,\tilde{\rho}_{i+1,i}$, defined by

$$\forall j \in \{1, \dots, i-1\} : \widetilde{\rho}_{i+1,j} = \rho_{i,j}$$

and

$$\widetilde{\rho}_{i+1,i} = \frac{x_{i+1}}{x_i + x_{i+1}} \rho_{i,i-1} + \sigma \sqrt{\frac{x_i x_{i+1}}{x_i + x_{i+1}}} \xi,$$

shows that the desired assertion holds for i + 1.

This finishes the proof.

Lemma 3.2. Fix everything as in the first two paragraphs of section 1. Then, for each $i \in \{2, ..., L\}$, there exist fixed continuous random variables $\sigma_{i,1}, \sigma_{i,2}, ..., \sigma_{i,i-1}$, only depending on γ , σ and the k_j , such that, for all $n \in \mathbb{N}_0$ and $x \in \mathbb{R}$,

$$\mathcal{N}_{n,i}(x) = \mathbb{E}\left[\prod_{j=1}^{i-1} (1-\psi) \left(\frac{k_j^{1-\gamma}}{k_i} n^{-\gamma} x + \sigma_{i,j} n^{\frac{1}{2}-\gamma}\right)\right].$$

Proof. Applying Lemma 3.1 to the strictly positive numbers $k_1, k_2 - k_1, \ldots, k_i - k_{i-1}$, reveals the existence of fixed continuous random variables $\rho_{i,1}, \ldots, \rho_{i,i-1}$, only depending on σ and the k_j , such that, by (3.1), keeping the notations (2.4), (2.7), (2.9) and (2.10) in mind,

$$\mathcal{N}_{n,i}(x) = \mathbb{E}\left[\prod_{j=1}^{i-1} \left(1 - \psi_{m_{n,j}}\right) \left(\frac{k_j}{k_i} x + \rho_{i,j} \sqrt{n}\right)\right],$$

which, by (2.6),

$$= \mathbb{E}\left[\prod_{j=1}^{i-1} (1-\psi) \left(\frac{k_j^{1-\gamma}}{k_i} n^{-\gamma} x + \frac{\rho_{i,j}}{k_j^{\gamma}} n^{\frac{1}{2}-\gamma}\right)\right],$$

which, putting $\sigma_{i,j} = \frac{
ho_{i,j}}{k_i^{\gamma}}$, proves the desired result.

Theorem 3.1. Fix everything as in the first two paragraphs of section 1. Then there exist fixed continuous random variables $\alpha_1, \ldots, \alpha_L$ and $\gamma_1, \ldots, \gamma_L$, only depending on γ , σ and the k_j , and, for all $i \in \{2, \ldots, L\}$ and $j \in \{1, \ldots, i-1\}$, fixed continuous random variables $\beta_{i,j}$ and $\delta_{i,j}$, only depending on γ , σ and the k_j ,

and a standard normally distributed random variable ξ , such that, for each $n \in \mathbb{N}_0$ and each bounded Borel measurable test function $h : \mathbb{R} \to \mathbb{R}$,

$$\mathbb{E}\left[\left\{h(\xi) - h\left(\frac{\sqrt{N_n}}{\sigma}\left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right] = \sum_{i=1}^{L} \mathbb{E}\left[h(\xi)\left\{\mathcal{R}_i(n) - \widetilde{\mathcal{R}}_i(n)\right\}\right],$$

with

$$\mathcal{R}_{i}(n) = \psi \left(k_{i}^{1-\gamma} n^{1-\gamma} \mu + \alpha_{i} n^{\frac{1}{2}-\gamma} \right) \prod_{j=1}^{i-1} (1-\psi) \left(k_{j}^{1-\gamma} n^{1-\gamma} \mu + \beta_{i,j} n^{\frac{1}{2}-\gamma} \right)$$

and

$$\widetilde{\mathcal{R}}_{i}(n) = \psi \left(k_{i}^{1-\gamma} n^{1-\gamma} \mu + \gamma_{i} n^{\frac{1}{2}-\gamma} \right) \prod_{j=1}^{i-1} (1-\psi) \left(k_{j}^{1-\gamma} n^{1-\gamma} \mu + \delta_{i,j} n^{\frac{1}{2}-\gamma} \right),$$

the empty product being 1.

Proof. By Lemma 3.2, for each $i \in \{2, ..., L\}$, there exists a fixed collection $\sigma_{i,1}, \sigma_{i,2}, ..., \sigma_{i,i-1}$ of continuous random variables, only depending on γ , σ and the k_i , such that, for all $n \in \mathbb{N}_0$ and $x \in \mathbb{R}$,

$$\mathcal{N}_{n,i}(x) = \mathbb{E}\left[\prod_{j=1}^{i-1} (1 - \psi) \left(\frac{k_j^{1-\gamma}}{k_i} n^{-\gamma} x + \sigma_{i,j} n^{\frac{1}{2} - \gamma}\right)\right].$$
(3.5)

Then fix stochastically independent standard normally distributed random variables ξ and η , each stochastically independent of all the $\sigma_{i,j}$. By Theorem 2.2,

$$\mathbb{E}\left[\left\{h(\xi) - h\left(\frac{\sqrt{N_n}}{\sigma}\left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right] = \sum_{i=1}^{L} \mathbb{E}\left[h(\xi)\left\{\mathcal{M}_i(n) - \widetilde{\mathcal{M}}_i(n)\right\}\right],\tag{3.6}$$

with

$$\mathcal{M}_{i}(n) = \left(\psi_{m_{n,i}} \mathcal{N}_{n,i}\right) \left(\mu m_{n,i} + \sigma \sqrt{m_{n,i}} \xi\right) \tag{3.7}$$

and

$$\widetilde{\mathcal{M}}_{i}(n) = \left(\psi_{m_{n,i}} \mathcal{N}_{n,i}\right) \left(\mu m_{n,i} + \sigma \sqrt{\frac{m_{n,i}(M_{n} - m_{n,i})}{M_{n}}} \xi + \sigma \frac{m_{n,i}}{\sqrt{M_{n}}} \eta\right). \tag{3.8}$$

Combining (2.8), (3.5), (3.7), (2.4) and (2.6), reveals that, for each $i \in \{1, ..., L\}$,

$$\mathbb{E}\left[h(\xi)\mathcal{M}_i(n)\right]$$

can be written as the expected value of the product with factors

$$h(\xi)\psi_{m_{n,i}}(\mu m_{n,i} + \sigma \sqrt{m_{n,i}}\xi)$$

$$= h(\xi)\psi\left(m_{n,i}^{1-\gamma}\mu + \sigma m_{n,i}^{\frac{1}{2}-\gamma}\right)$$

$$= h(\xi)\psi\left(k_i^{1-\gamma}n^{1-\gamma}\mu + \sigma k_i^{\frac{1}{2}-\gamma}\xi n^{\frac{1}{2}-\gamma}\right)$$
(3.9)

and

$$\prod_{j=1}^{i-1} (1 - \psi) \left(\frac{k_j^{1-\gamma}}{k_i} n^{-\gamma} \left(\mu m_{n,i} + \sigma \sqrt{m_{n,i}} \xi \right) + \sigma_{i,j} n^{\frac{1}{2} - \gamma} \right) \\
= \prod_{j=1}^{i-1} (1 - \psi) \left(k_j^{1-\gamma} n^{1-\gamma} \mu + \left(\sigma \frac{k_j^{1-\gamma}}{\sqrt{k_i}} \xi + \sigma_{i,j} \right) n^{\frac{1}{2} - \gamma} \right),$$
(3.10)

the empty product being 1. Analogously, combining (2.8), (3.5), (3.8), (2.4), (2.5) and (2.6), shows that, for each $i \in \{1, ..., L\}$,

$$\mathbb{E}\left[h(\xi)\widetilde{\mathcal{M}}_i(n)\right]$$

can be written as the expected value of the product with factors

$$h(\xi)\psi_{m_{n,i}}\left(\mu m_{n,i} + \sigma\sqrt{\frac{m_{n,i}(M_n - m_{n,i})}{M_n}}\xi + \sigma\frac{m_{n,i}}{\sqrt{M_n}}\eta\right)$$

$$= h(\xi)\psi\left(m_{n,i}^{1-\gamma}\mu + \sigma\sqrt{\frac{M_n - m_{n,i}}{M_n}}m_{n,i}^{\frac{1}{2}-\gamma}\xi + \sigma\sqrt{\frac{m_{n,i}}{M_n}}m_{n,i}^{\frac{1}{2}-\gamma}\eta\right)$$

$$= h(\xi)\psi\left(k_i^{1-\gamma}n^{1-\gamma}\mu + \sigma k_i^{\frac{1}{2}-\gamma}\left(\sqrt{\frac{k_{L+1} - k_i}{k_{L+1}}}\xi + \sqrt{\frac{k_i}{k_{L+1}}}\eta\right)n^{\frac{1}{2}-\gamma}\right)$$
(3.11)

and

$$\prod_{j=1}^{i-1} (1 - \psi) \left(\frac{k_j^{1-\gamma}}{k_i} n^{-\gamma} \left(\mu m_{n,i} + \sigma \sqrt{\frac{m_{n,i} (M_n - m_{n,i})}{M_n}} \xi + \sigma \frac{m_{n,i}}{\sqrt{M_n}} \eta \right) + \sigma_{i,j} n^{\frac{1}{2} - \gamma} \right) \\
= \prod_{j=1}^{i-1} (1 - \psi) \left(k_j^{1-\gamma} n^{1-\gamma} \mu + \left\{ \sigma \frac{k_j^{1-\gamma}}{\sqrt{k_i}} \left(\sqrt{\frac{k_{L+1} - k_i}{k_{L+1}}} \xi + \sqrt{\frac{k_i}{k_{L+1}}} \eta \right) + \sigma_{i,j} \right\} n^{\frac{1}{2} - \gamma} \right), (3.12)$$

the empty product being 1. Now, for $i \in \{1, ..., L\}$, put in (3.9)

$$\alpha_i = \sigma k_i^{\frac{1}{2} - \gamma} \xi,$$

for $i \in \{2, \dots, L\}$ and $j \in \{1, \dots, i-1\}$, put in (3.10)

$$\beta_{i,j} = \sigma \frac{k_j^{1-\gamma}}{\sqrt{k_i}} \xi + \sigma_{i,j},$$

for $i \in \{1, ..., L\}$, put in (3.11)

$$\gamma_i = \sigma k_i^{\frac{1}{2} - \gamma} \left(\sqrt{\frac{k_{L+1} - k_i}{k_{L+1}}} \xi + \sqrt{\frac{k_i}{k_{L+1}}} \eta \right),$$

and, for $i \in \{2, ..., L\}$ and $j \in \{1, ..., i-1\}$, put in (3.12)

$$\delta_{i,j} = \sigma \frac{k_j^{1-\gamma}}{\sqrt{k_i}} \left(\sqrt{\frac{k_{L+1} - k_i}{k_{L+1}}} \xi + \sqrt{\frac{k_i}{k_{L+1}}} \eta \right) + \sigma_{i,j}.$$

This allows us to conclude from (3.6) that the desired equation holds.

In the next section, we will derive an asymptotic normality result for $\widehat{\mu}_{N_n}$ from Theorem 3.1.

4. THE MAIN RESULT

Recall that the total variation distance between random variables X and Y is given by

$$d_{TV}(X,Y) = \sup_{A} |\mathbb{P}[X \in A] - \mathbb{P}[Y \in A]|,$$

the supremum running over all Borel sets $A \subset \mathbb{R}$. It is well known that convergence for the total variation distance is strictly stronger than weak convergence. For more information on this distance, we refer the reader to Rachev (1991) and Zolotarev (1983).

We are now in a position to state and prove the main result of this paper.

Theorem 4.1. Fix everything as in the first two paragraphs of section 1. Furthermore, consider a standard normally distributed random variable ξ and the sample mean $\widehat{\mu}_{N_n} = K_{N_n}/N_n$. Then

$$d_{TV}\left(\xi, \frac{\sqrt{N_n}}{\sigma}\left(\widehat{\mu}_{N_n} - \mu\right)\right) \to 0 \text{ as } n \to \infty$$
 (4.1)

in each of the following cases:

- (A) $\gamma > 1$ and ψ has a finite limit in 0,
- (B) $\gamma = 1$ and ψ has a finite limit in μ ,
- (C) (1) $1/2 < \gamma < 1$, $\mu \neq 0$, and ψ has finite limits in $-\infty$ and ∞ ,
 - (2) $1/2 < \gamma < 1$, $\mu = 0$, and ψ has a finite limit in 0,
- (D) $\gamma = 1/2$, $\mu \neq 0$, and ψ has finite limits in $-\infty$ and ∞ ,
- (E) (1) $0 \le \gamma < 1/2$, $\mu \ne 0$, and ψ has finite limits in $-\infty$ and ∞ ,
 - (2) $0 \le \gamma < 1/2$, $\mu = 0$, and ψ has coinciding finite limits in $-\infty$ and ∞ .

In particular, letting Φ be the standard normal cdf, it holds for each $x \in \mathbb{R}_0^+$ that

$$\left| 2\Phi(x) - 1 - \mathbb{P}\left[\widehat{\mu}_{N_n} - \frac{\sigma}{\sqrt{N_n}} x \le \mu \le \widehat{\mu}_{N_n} + \frac{\sigma}{\sqrt{N_n}} x \right] \right| \to 0 \text{ as } n \to \infty$$
 (4.2)

in each of the cases (A)–(E), i.e. confidence intervals for μ based on $\widehat{\mu}_{N_n}$ are often reliable if n is large enough.

Remark 4.1. Our stopping rule (1.1) is designed in such a way that it analyzes the sum of the observations based on the null hypothesis $\mu=0$. This becomes clear if we take ψ of the form (1.2). Indeed, in this case, the trial is stopped (to reject the null hypothesis $\mu=0$) at the first $k_i n$ for which $|K_{k_i n}| \geq C(k_i n)^{\gamma}$. Therefore, the distinction between $\mu=0$ and $\mu\neq 0$ in Theorem 4.1 is natural. Of course, it is possible to effortlessly switch to the null hypothesis $\mu=\mu_0$ for a different parameter $\mu_0\in\mathbb{R}_0$, by considering the data $X_1-\mu_0,X_2-\mu_0,\ldots$

Remark 4.2. In the case where $\gamma=1/2$ and $\mu=0$, we have not stated an asymptotic normality result. In the next section, we will show that such a result fails to hold (Example 5.1). This is not a severe drawback, because the case $\gamma=1/2$ corresponds to the Pocock boundary, which is very rarely used in practice, often in favor of the more popular O'Brien-Fleming boundary, because it tends to assign too much type I error at early looks. In other words, it too generously allows for very early stopping (Whitehead (1987)).

Proof of Theorem 4.1. By Theorem 3.1, fix continuous random variables $\alpha_1, \ldots, \alpha_L$ and $\gamma_1, \ldots, \gamma_L$, only depending on γ , σ and the k_j , and, for all $i \in \{2, \ldots, L\}$ and $j \in \{1, \ldots, i-1\}$, continuous random variables $\beta_{i,j}$ and $\delta_{i,j}$, only depending on γ , σ and the k_j , and a standard normally distributed random variable ξ_0 , such that, for each $n \in \mathbb{N}_0$ and each Borel measurable set $A \subset \mathbb{R}$,

$$\mathbb{E}\left[\left\{1_{A}(\xi_{0})-1_{A}\left(\frac{\sqrt{N_{n}}}{\sigma}\left(\widehat{\mu}_{N_{n}}-\mu\right)\right)\right\}\right]=\sum_{i=1}^{L}\mathbb{E}\left[1_{A}(\xi_{0})\left\{\mathcal{R}_{i}(n)-\widetilde{\mathcal{R}}_{i}(n)\right\}\right],\tag{4.3}$$

with

$$\mathcal{R}_{i}(n) = \psi \left(k_{i}^{1-\gamma} n^{1-\gamma} \mu + \alpha_{i} n^{\frac{1}{2}-\gamma} \right) \prod_{j=1}^{i-1} (1-\psi) \left(k_{j}^{1-\gamma} n^{1-\gamma} \mu + \beta_{i,j} n^{\frac{1}{2}-\gamma} \right)$$
(4.4)

and

$$\widetilde{\mathcal{R}}_{i}(n) = \psi \left(k_{i}^{1-\gamma} n^{1-\gamma} \mu + \gamma_{i} n^{\frac{1}{2}-\gamma} \right) \prod_{j=1}^{i-1} (1-\psi) \left(k_{j}^{1-\gamma} n^{1-\gamma} \mu + \delta_{i,j} n^{\frac{1}{2}-\gamma} \right), \tag{4.5}$$

the empty product being 1. Since ξ and ξ_0 have the same distribution, we infer from (4.3) that the upper bound

$$d_{TV}\left(\xi, \frac{\sqrt{N_n}}{\sigma} \left(\widehat{\mu}_{N_n} - \mu\right)\right) \le \sum_{i=1}^{L} \mathbb{E}\left[\left|\mathcal{R}_i(n) - \widetilde{\mathcal{R}}_i(n)\right|\right]$$
(4.6)

holds for each $n \in \mathbb{N}_0$. The fact that limit relation (4.1) holds in each of the cases (A)–(E), can be easily read off from the upper bound (4.6) and the expressions (4.4) and (4.5).

Suppose, for instance, that we are in the case (E) (2), i.e. $0 \le \gamma < 1/2$, $\mu = 0$, and ψ has coinciding finite limits in $-\infty$ and ∞ , say with value λ . The α_i , $\beta_{i,j}$, γ_i and $\delta_{i,j}$ being continuous, they all differ from zero outside a fixed event with probability zero. Thus, almost surely, each of the expressions $\alpha_i n^{\frac{1}{2} - \gamma}$, $\beta_{i,j} n^{\frac{1}{2} - \gamma}$, $\gamma_i n^{\frac{1}{2} - \gamma}$ and $\delta_{i,j} n^{\frac{1}{2} - \gamma}$ tends to either $-\infty$ or ∞ as $n \to \infty$, whence, by (4.4) and (4.5), almost surely, $\mathcal{R}_i(n)$ and $\widetilde{\mathcal{R}}_i(n)$ both tend to $\lambda(1 - \lambda)^{i-1}$ as $n \to \infty$. We conclude from the dominated convergence theorem that the upper bound in (4.6) tends to 0.

The other cases are analyzed analogously.

Finally, for each $x \in \mathbb{R}_0^+$, considering the Borel set A = [-x, x], allows us to derive (4.2) from (4.1), which finishes the proof.

Corollary 4.1. Fix everything as in the first two paragraphs of section 1, and assume in addition that ψ takes the form (1.2) and $\mu \notin \{-C, C\}$. Then always

$$d_{TV}\left(N(0,1), \frac{\sqrt{N_n}}{\sigma}\left(\widehat{\mu}_{N_n} - \mu\right)\right) \to 0 \text{ as } n \to \infty,$$

except in the case where $\gamma = 1/2$ and $\mu = 0$. In particular, letting Φ be the standard normal cdf, it always holds that, for each $x \in \mathbb{R}_0^+$,

$$\left|2\Phi(x)-1-\mathbb{P}\left[\widehat{\mu}_{N_n}-\frac{\sigma}{\sqrt{N_n}}x\leq \mu\leq \widehat{\mu}_{N_n}+\frac{\sigma}{\sqrt{N_n}}x\right]\right|\to 0 \ as \ n\to\infty,$$

except in the case where $\gamma = 1/2$ and $\mu = 0$.

Proof. This is an easy application of Theorem 4.1.

Corollary 4.1 shows that in the important situation of a group sequential trial with outcomes with law $N(\mu, \sigma^2)$, which is stopped either at the first $k_i n$ for which $|K_{k_i n}| \ge C(k_i n)^{\gamma}$ or at $k_{L+1} n$, naive confidence intervals for μ , based on the ordinary sample mean $\widehat{\mu}_{N_n}$, are reliable for large n if $\mu \notin \{-C, C\}$ and $(\gamma, \mu) \ne (1/2, 0)$. We will illustrate this with simulations in section 6.

In the next section, we will provide some examples, which show that the conditions under which Theorem 4.1 holds, cannot be omitted.

5. SOME EXAMPLES

In this section, we take $\mu=0$, $\sigma=1$, L=1, $k_1=1$ and $k_2=2$. Furthermore, we fix independent random variables ξ and η with law N(0,1). Then it follows from Theorem 2.2, and (2.4), (2.5) and (2.6), that, for each $n \in \mathbb{N}_0$ and each bounded Borel measurable test function $h: \mathbb{R} \to \mathbb{R}$,

$$\mathbb{E}\left[\left\{h(\xi) - h\left(\sqrt{N_n}\left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right]$$

$$= \mathbb{E}\left[h(\xi)\left\{\psi\left(\xi n^{\frac{1}{2}-\gamma}\right) - \psi\left(\frac{\sqrt{2}}{2}\left(\xi + \eta\right)n^{\frac{1}{2}-\gamma}\right)\right\}\right].$$
(5.1)

Recall that the Kolmogorov distance between random variables X and Y is given by

$$K(X,Y) = \sup_{x \in \mathbb{R}} |\mathbb{P}\left[X \le x\right] - \mathbb{P}\left[Y \le x\right]|.$$

It is well known that, for a continuous random variable X and a sequence of random variables $(Y_n)_n$, $K(X,Y_n) \to 0$ if and only if $(Y_n)_n$ converges weakly to X. For more information on this distance, we refer the reader to Rachev (1991) and Zolotarev (1983).

We will now derive two interesting examples from equation (5.1).

Example 5.1. Take $\gamma = 1/2$ and, for $C \in \mathbb{R}_0^+$, ψ of the form (1.2). Thus, for $n \in \mathbb{N}_0$, this example corresponds to a trial with independent standard normally distributed outcomes, of maximal length 2n, and in which one interim analysis is performed after having collected n data. The trial is stopped if the absolute value of the sum of the first n data exceeds $Cn^{1/2}$, and continued otherwise. Let, for $x \in \mathbb{R}$, $1_{]-\infty,x]}$ be the characteristic function of the set $]-\infty,x]$. Then, Φ being the standard normal cdf, a straightforward calculation allows us to derive from (5.1) that, for each $x \in \mathbb{R}$ and each $n \in \mathbb{N}_0$,

$$\mathbb{E}\left[\left\{1_{]-\infty,x]}(\xi) - 1_{]-\infty,x]}\left(\sqrt{N_n}\left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right]$$

$$= \mathbb{E}\left[1_{[-\infty,x]}(\xi)1_{]-C,C[}\left(\frac{\sqrt{2}}{2}(\xi+\eta)\right)\right] - \mathbb{E}\left[1_{]-\infty,x]}(\xi)1_{]-C,C[}(\xi)\right]$$

$$= \mathbb{E}\left[\Phi\left(\left(\sqrt{2}C - \eta\right) \wedge x\right) - \Phi\left(\left(-\sqrt{2}C - \eta\right) \wedge x\right)\right] - \left[\Phi\left(C \wedge x\right) - \Phi\left(-C \wedge x\right)\right],$$
(5.2)

 \wedge standing for the operation that takes the minimum of two numbers. In particular, taking x = -C in (5.2), it holds for each $n \in \mathbb{N}_0$ that

$$\mathbb{E}\left[\left\{1_{]-\infty,-C]}(\xi)-1_{]-\infty,-C]}\left(\sqrt{N_n}\left(\widehat{\mu}_{N_n}-\mu\right)\right)\right\}\right]$$

$$=\mathbb{E}\left[\Phi\left(\left(\sqrt{2}C-\eta\right)\wedge-C\right)-\Phi\left(\left(-\sqrt{2}C-\eta\right)\wedge-C\right)\right],$$

which, considering the event $\{0 \le \eta \le \sqrt{2}C\}$,

$$\geq \quad \mathbb{P}\left[0 \leq \eta \leq \sqrt{2}C\right] \left[\Phi(-C) - \Phi\left(-\sqrt{4}C\right)\right]$$

$$= \quad \left[\Phi\left(\sqrt{2}C\right) - \Phi(0)\right] \left[\Phi\left(-C\right) - \Phi\left(-\sqrt{4}C\right)\right] > 0,$$

from which we conclude that

$$\begin{split} &K\left(\xi,\sqrt{N_{n}}\left(\widehat{\mu}_{N_{n}}-\mu\right)\right) \\ &= \sup_{x\in\mathbb{R}}\left|\mathbb{E}\left[\Phi\left(\left(\sqrt{2}C-\eta\right)\wedge x\right)-\Phi\left(\left(-\sqrt{2}C-\eta\right)\wedge x\right)\right]-\left[\Phi\left(C\wedge x\right)-\Phi\left(-C\wedge x\right)\right]\right| \\ &\geq \left[\Phi\left(\sqrt{2}C\right)-\Phi(0)\right]\left[\Phi\left(-C\right)-\Phi\left(-\sqrt{4}C\right)\right]>0. \end{split}$$

That is, for each $n \in \mathbb{N}_0$, the Kolmogorov distance between ξ and $\sqrt{N_n} (\widehat{\mu}_{N_n} - \mu)$ takes a strictly positive constant value. We infer that $(\sqrt{N_n} (\widehat{\mu}_{N_n} - \mu))_n$ fails to converge weakly to ξ . In particular, case (D) of Theorem 4.1 is not extendable to $\gamma = 1/2$ and $\mu = 0$, even if ψ has a finite limit in 0 and coinciding finite limits in $-\infty$ and ∞ .

Example 5.2. Take $\gamma \in \mathbb{R}_0^+$ arbitrary and $\psi = 1_{]-\infty,0]}$, the characteristic function of the set $]-\infty,0]$. Thus, for $n \in \mathbb{N}_0$, this example corresponds to a trial with independent standard normally distributed outcomes, of maximal length 2n, and in which one interim analysis is performed after having collected n data. The trial is stopped if the sum of the first n data is negative, and continued otherwise. Let, for $x \in \mathbb{R}$, $1_{]-\infty,x]}$ be the characteristic function of the set $]-\infty,x]$. Then, Φ being the standard normal cdf, a straightforward calculation allows us to derive from (5.1) that, for each $x \in \mathbb{R}$ and each $n \in \mathbb{N}_0$,

$$\mathbb{E}\left[\left\{1_{]-\infty,x]}(\xi) - 1_{]-\infty,x]} \left(\sqrt{N_n} \left(\widehat{\mu}_{N_n} - \mu\right)\right)\right\}\right] \\ = \mathbb{E}\left[1_{]-\infty,x]}(\xi)1_{]-\infty,0]}(\xi)\right] - \mathbb{E}\left[1_{]-\infty,x]}(\xi)1_{]-\infty,0]}(\xi + \eta)\right] \\ = \Phi(x \wedge 0) - \mathbb{E}\left[1_{]-\infty,x]}(\xi)\Phi(-\xi)\right] \\ = \Phi(x \wedge 0) - \Phi(x) + \Phi^2(x)/2,$$

 \land standing for the operation that takes the minimum of two numbers. We deduce that, for each $n \in \mathbb{N}_0$,

$$K\left(\xi, \sqrt{N_n} \left(\widehat{\mu}_{N_n} - \mu\right)\right) = \sup_{x \in \mathbb{P}} \left| \Phi(x \wedge 0) - \Phi(x) + \Phi^2(x)/2 \right| = 1/8.$$

We infer that $(\sqrt{N_n}(\widehat{\mu}_{N_n} - \mu))_n$ fails to converge weakly to ξ . This shows that in the cases (A), (B), (C) (2) and (E) (2) of Theorem 4.1, the conditions on ψ cannot be omitted.

6. SIMULATIONS

In order to illustrate Theorem 4.1 and Corollary 4.1, we have conducted the following simulation study. For $\mu \in \{-1,0,1\}$, $n \in \{10,50,100,500\}$, $C \in \{0,1,2\}$, and $\gamma \in \{0,0.25,0.5,0.75,1,2\}$, we have simulated a group sequential trial with the following properties.

- 1. Independent observations with distribution $N(\mu, 1)$ are collected.
- 2. Interim analyses of the sum of the data are performed at n and 2n.
- 3. (a) For the one-sided stopping rule, the trial is stopped either at the first in, where $i \in \{1, 2\}$, for which

$$\sum_{k=1}^{in} X_k \ge C(in)^{\gamma},\tag{6.1}$$

or at 3n.

(b) For the two-sided stopping rule, the trial is stopped either at the first in, where $i \in \{1, 2\}$, for which

$$\left| \sum_{k=1}^{in} X_k \right| \ge C(in)^{\gamma},\tag{6.2}$$

or at 3n.

Notice that the final sample size N_n of the above trial can take the values n, 2n, and 3n. Furthermore, the above stopping rules are special cases of the general stopping rule (1.1), where the one-sided stopping rule (6.1) corresponds to the choice

$$\psi_{C,1}(x) = \begin{cases} 1 & \text{if} \quad x \ge C \\ 0 & \text{if} \quad x < C \end{cases}, \tag{6.3}$$

and the two-sided stopping rule (6.2) to the choice

$$\psi_{C,2}(x) = \begin{cases} 1 & \text{if} \quad |x| \ge C \\ 0 & \text{if} \quad |x| < C \end{cases}$$
 (6.4)

For each fixed choice of the parameters μ , n, C, and γ , we have calculated the following values for the sample mean $\widehat{\mu}_{N_n} = \frac{1}{N_n} \sum_{k=1}^{N_n} X_k$ for the stopping rules (6.1) and (6.2):

- 1. the average lower confidence limit, the average upper confidence limit, and the true coverage probability for the interval $[\hat{\mu}_{N_n} 1.96/\sqrt{N_n}, \hat{\mu}_{N_n} + 1.96/\sqrt{N_n}]$, which would be a 95% confidence interval for μ if $\sqrt{N_n}(\hat{\mu}_{N_n} \mu)$ were standard normally distributed,
- 2. the *Kolmogorov distance* between the empirical distribution of $\sqrt{N_n}(\widehat{\mu}_{N_n} \mu)$ and the standard normal distribution, which is close to 0 if and only if $\sqrt{N_n}(\widehat{\mu}_{N_n} \mu)$ is close to being standard normally distributed.
- 3. the average length of the trial.

From the calculated numbers, which can be found in Table 2 of the appendix, we can draw the following conclusions.

1. For $n \ge 50$, the true coverage probability of the interval

$$\left[\widehat{\mu}_{N_n} - 1.96/\sqrt{N_n}, \widehat{\mu}_{N_n} + 1.96/\sqrt{N_n}\right]$$

is in all cases close to 95%. So using this type of naive confidence interval after a group sequential trial turns out to be a reliable method.

2. Asymptotic normality of the quantity $\sqrt{N_n}(\widehat{\mu}_{N_n}-\mu)$ is more subtle. In many cases, the Kolmogorov distance between the empirical distribution of $\sqrt{N_n}(\widehat{\mu}_{N_n}-\mu)$ and the standard normal distribution is already below 0.05 for n=50, implying that the naively normalized sample mean is close to asymptotic normality. However, there are a few exceptions for which the Kolmogorov distance is substantially larger than 0.05 for n=50. These exceptions are listed in Table 1 below. If an exception turns out to be a case in which Theorem 4.1 guarantees asymptotic normality, we have mentioned this.

Table 1. Cases where the Kolmogorov distance is large for $n =$	Table 1.	Cases w	here the F	Kolmogorov	distance i	is large	for $n = \frac{1}{2}$	50
--	----------	---------	------------	------------	------------	----------	-----------------------	----

μ	C	γ	one- or two-sided	Kol. Dist.	case in Theorem 4.1
0	2	0	two-sided	0.111	E (2)
0	2	0.25	two-sided	0.147	E(2)
0	2	0	one-sided	0.176	/
0	2	0.25	one-sided	0.130	/
-1	1	1	two-sided	0.190	/
0	1	0	two-sided	0.075	E(2)
0	1	0.25	two-sided	0.136	E(2)
0	1	0.5	two-sided	0.118	/
1	1	1	two-sided	0.187	/
0	1	0	one-sided	0.183	/
0	1	0.25	one-sided	0.158	/
0	1	0.5	one-sided	0.126	1
1	1	1	one-sided	0.187	/
0	0	arbitrary	one-sided	0.187	/

We conclude that the quantity $\sqrt{N_n}(\widehat{\mu}_{N_n} - \mu)$ is close to a standard normal distribution for n = 50 in all cases in which Theorem 4.1 guarantees asymptotic normality, except in the case E (2). Indeed, E (2) is the only case in which asymptotic normality is reached more slowly.

7. CONCLUDING REMARKS

In this paper, we have studied a broad class of group sequential trials, with random length N_n , in which independent observations X_1, X_2, \ldots with law $N(\mu, \sigma^2)$ are collected, and in which interim analyses of the sum of the observations are performed. After each interim analysis, one decides whether the trial is stopped or continued, based on the stopping rule (1.1), with ψ a fixed Borel measurable map of $\mathbb R$ into $[0,1], \gamma \in \mathbb R_0^+$ a fixed shape parameter, and, for $m \in \mathbb N_0$, K_m the sum of the first m observations. We have illustrated that this mathematical model contains several interesting settings, which have been studied extensively in the literature. In particular, the choice $\gamma = 1/2$ leads to the Pocock boundaries, and the choice $\gamma = 0$ to the O'Brien-Fleming boundaries.

In the above described group sequential trial setting, we have studied the asymptotic distribution of the sample mean $\widehat{\mu}_{N_n} = K_{N_n}/N_n$, where, as $n \to \infty$, the maximal number of observations in the trial increases to infinity, while the number L of interim analyses is kept fixed, and, for every $i \in \{1, \ldots, L\}$, the ratio of the number of observations collected at the i-th interim analysis to the maximal number of observations is also kept fixed.

We have shown in Theorem 4.1, our main result, that, in many realistic cases, the quantity $\frac{\sqrt{N_n}}{\sigma} \left(\widehat{\mu}_{N_n} - \mu \right)$ is asymptotically normal for the total variation distance, from which we have derived that it is often safe to rely on confidence intervals of the type $\left[\widehat{\mu}_{N_n} - \frac{\sigma}{\sqrt{N_n}} x, \widehat{\mu}_{N_n} + \frac{\sigma}{\sqrt{N_n}} x \right]$ for μ . A simulation study has confirmed our theoretical findings.

ACKNOWLEDGEMENTS

We thank the editor and the anonymous referee for carefully reading the manuscript and providing valuable comments

We are grateful to the Fund for Scientific Research of Flanders (FWO) for providing Ben Berckmoes with a postdoctoral fellowship.

Financial support from the IAP research networking icy) is gratefully acknowledged.	k #P7/06 of the Belgian Gover	rnment (Belgian Science Pol-

REFERENCES

- Berckmoes, B., Ivanova, A., and Molenberghs, G. (2018) On the Sample Mean after a Group Sequential Trial, Computational Statistics & Data Analysis 125:104-118.
- Chang, M. N. (1989) Confidence Intervals for a Normal Mean following a Group Sequential Test, Biometrics 45:247-254.
- Molenberghs, G., Kenward, M. G., Aerts, M., Verbeke, G., Tsiatis, A. A., Davidian, M., and Rizopoulos, D. (2014) On Random Sample Size, Ignorability, Ancillarity, Completeness, Separability, and Degeneracy: Sequential Trials, Random Sample Sizes, and Missing Data, Statistical Methods in Medical Research 23:11-41.
- O'Brien, P. C. and Fleming, T. R. (1979). A Multiple Testing Procedure for Clinical Trials, Biometrics 35:549-556.
- Pocock, S. J. (1977) Group Sequential Methods in the Design and Analysis of Clinical Trials, Biometrika 64:191-199.
- Rachev, S. T. (1991) *Probability Metrics and the Stability of Stochastic Models*, Chichester: John Wiley & Sons.
- Siegmund, D. (1978). Estimation following Sequential Tests, Biometrika 65:341-349.
- Whitehead, J. (1987). The Design and Analysis of Sequential Clinical Trials, Chichester: John Wiley & Sons.
- Woodroofe, M. (1992) Estimation after Sequential Testing: a Simple Approach for a Truncated Sequential Probability Ratio Test, Biometrika 79:347-353.
- Zolotarev, V. M. (1983) Probability Metrics (Russian) Teoriya Veroyatnostei i ee Primeneniya 28:264-287.

APPENDIX

Table 2: Simulation results for the normal case with the number of simulated i.i.d. draws per sample 400, the number of simulated samples 1000. Values for standard deviation is kept fixed, $\sigma=1$. CL: confidence limit. Cov.Prob: coverage probability. Kol.Dist.: Kolmogorov distance.

$=$ μ	\overline{n}	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size
			<u> </u>		no stopping			
-1				-1.098	-0.902	0.955	0.021	400
0				-0.098	0.098	0.955	0.021	400
1				0.902	1.098	0.955	0.021	400
				t	wo-sided rule			
-1	10	2	0	-1.602	-0.403	0.914	0.019	10
-1	10	2	0.25	-1.603	-0.407	0.919	0.019	10
-1	10	2	0.50	-1.612	-0.453	0.926	0.056	11
-1	10	2	0.75	-1.547	-0.625	0.923	0.131	20
-1	10	2	1	-1.358	-0.647	0.939	0.018	30
-1	10	2	2	-1.357	-0.647	0.939	0.018	30
0	10	2	0	-0.502	0.503	0.906	0.126	17
0	10	2	0.25	-0.435	0.429	0.897	0.109	23
0	10	2	0.50	-0.372	0.360	0.900	0.036	29
0	10	2	0.75	-0.357	0.354	0.938	0.018	30
0	10	2	1	-0.357	0.353	0.939	0.018	30
0	10	2	2	-0.357	0.353	0.939	0.018	30
1	10	2	0	0.405	1.604	0.915	0.019	10
1	10	2	0.25	0.414	1.607	0.925	0.019	10
1	10	2	0.50	0.456	1.618	0.942	0.064	11
1	10	2	0.75	0.628	1.552	0.926	0.139	20
1	10	2	1	0.644	1.355	0.937	0.018	30
1	10	2	2	0.643	1.353	0.939	0.018	30
					one-sided rule			
-1	10	2	0	-1.357	-0.647	0.939	0.018	30
-1	10	2	0.25	-1.357	-0.647	0.939	0.018	30
-1	10	2	0.50	-1.357	-0.647	0.939	0.018	30
-1	10	2	0.75	-1.357	-0.647	0.939	0.018	30
-1	10	2	1	-1.357	-0.647	0.939	0.018	30
-1	10	2	2	-1.357	-0.647	0.939	0.018	30
0	10	2	0	-0.351	0.509	0.924	0.149	23
0	10	2	0.25	-0.340	0.445	0.919	0.099	26
0	10	2	0.50	-0.350	0.369	0.922	0.026	29
0	10	2	0.75	-0.357	0.354	0.938	0.018	30
0	10	2	1	-0.357	0.353	0.939	0.018	30
0	10	2	2	-0.357	0.353	0.939	0.018	30
1	10	2	0	0.405	1.604	0.915	0.019	10

Table 2 – *Continued from previous page*

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					lable 2 – Con				
1 10	μ	n	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size
1 10 2 0.75 0.628 1.552 0.926 0.139 20 1 10 2 1 0.644 1.355 0.937 0.018 30 1 10 2 2 0.643 1.353 0.939 0.018 30 1 10 2 2 0.644 1.355 0.937 0.018 30	1	10	2	0.25	0.414	1.607	0.925	0.019	10
1 10 2 1 0.644 1.355 0.937 0.018 30 1 10 2 2 0.643 1.353 0.939 0.018 30	1	10	2	0.50	0.456	1.618	0.942	0.064	11
1 10 2 2 0.643 1.353 0.939 0.018 30	1	10	2	0.75	0.628	1.552	0.926	0.139	20
Two-sided rule	1	10	2	1	0.644	1.355	0.937	0.018	30
-1 50 2 0 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.25 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.50 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.50 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.75 -1.282 -0.736 0.958 0.036 52 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.50 -0.165 0.166 0.913 0.020 150 0 50 2 0.50 -0.165 0.166 0.913 0.020 150 0 50 2 0.50 -0.165 0.166 0.957 0.020 150 0 50 2 0.50 -0.165 0.161 0.957 0.020 150 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 0.839 0.957 0.020 150 1 50 2 0.50 0.721 0.839 0.957 0.020 150 1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -0.159 0.161 0.957 0.020 150 -1 50 2 0.75 -0.159 0.161 0.957 0.020 150 -1 50 2 0.75 -0.159 0.161 0.957 0.020 150 -1 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.50 -0.157 0.169 0.936 0.020 150 -1 50 2 0.75 -0.159 0.161 0.957 0.020 150 -1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.751 1.273 0.939 0.023 50 1 50 2 0.50 0.751 1.273 0.939 0.023 50 1 50 2 0.50 0.751 1.273 0.939 0.023 50 1 50 2 0.50 0.751 1.273 0.939 0.023 50 1 50 2 0.50 0.751 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0	1	10	2	2	0.643	1.353	0.939	0.018	30
-1 50 2 0.25 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.50 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.75 -1.282 -0.736 0.958 0.036 52 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 0.75 0.159 0.161 0.957 0.020 150 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.55 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -0.721 0.200 0.957 0.020 150 -1 50 2 0.50 0.721 0.200 0.957 0.020 150 -1 50 2 0.50 0.721 0.200 0.957 0.020 150 -1 50 2 0.50 0.721 0.200 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.740 0.957 0.020 150 -1 50 2 0.50 0.7					t	wo-sided rul	e		
-1 50 2 0.50 -1.279 -0.727 0.939 0.023 50 -1 50 2 0.75 -1.282 -0.736 0.958 0.036 52 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.50 0.721 0.273 0.939 0.023 50 1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.50 0.721 0.273 0.939 0.023 50 -1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.731 0.039 0.957 0.020 150 -1 50 2 0.50 0.75 0.159 0.060 0.957 0.020 150 -1 50 2 0.75 0.159 0.061 0.957 0.020 150 -1 50 2 0.75 0.159 0.061 0.957 0.020 150 -1 50 2 0.75 0.159 0.161 0.957 0.020 150 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.50 0.721 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 50 2 0.75 0.731 1.273 0.939 0.023 50 -1 5	-1	50	2	0	-1.279	-0.727	0.939	0.023	50
-1 50 2 0.75 -1.282 -0.736 0.958 0.036 52 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 0.75 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 0.841 0.957 0.020 150 1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.943 0.020 150 0 50 2 0.50 -0.157 0.169 0.943 0.020 150 0 50 2 0.50 -0.159 0.161 0.957 0.020 150 0 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.50 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.50 0.75 0.731 1.276 0.955 0.026 52	-1	50	2	0.25	-1.279	-0.727	0.939	0.023	50
-1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -0.50 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.50 -0.159 0.161 0.957 0.020 150 0 50 2 0.50 -0.159 0.161 0.957 0.020 150 0 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.75 0.731 1.276 0.955 0.026 52	-1	50	2	0.50	-1.279	-0.727	0.939	0.023	50
-1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0.25 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.262 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 2 0.75 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 0.841 1.161 0.957 0.020 150 0 50 2 1 0.841 1.161 0.957 0.020 150 0 50 2 1 0.841 1.161 0.957 0.020 150 0 50 2 2 0.050 0.721 0.273 0.939 0.023 50 0.026 52 0.026 0	-1	50	2	0.75	-1.282	-0.736	0.958	0.036	52
0 50 2 0 -0.262 0.255 0.938 0.111 62 0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273	-1	50	2	1	-1.159	-0.839	0.957	0.020	150
0 50 2 0.25 -0.226 0.217 0.928 0.147 93 0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0	-1	50	2	2	-1.159	-0.839	0.957	0.020	150
0 50 2 0.50 -0.165 0.166 0.913 0.020 145 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.75 0.731 1.161 0.957 0.020 150 1 50 2 0.841 1.161 0.957 <	0	50	2	0	-0.262	0.255	0.938	0.111	62
0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 0.75 0.731 1.161 0.957 0.020 150 1 50 2 0.841 1.161 0.957 <td< td=""><td>0</td><td>50</td><td>2</td><td>0.25</td><td>-0.226</td><td>0.217</td><td>0.928</td><td>0.147</td><td>93</td></td<>	0	50	2	0.25	-0.226	0.217	0.928	0.147	93
0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 0 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.	0	50	2	0.50	-0.165	0.166	0.913	0.020	145
0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 cone-sided rule	0	50	2	0.75	-0.159	0.161	0.957	0.020	150
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0	50	2	1	-0.159	0.161	0.957	0.020	150
1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 tone-sided rule one-sided rule tone-sided rule one-sided rule tone-sided rule tone-sided rule one-sided rule tone-sided rule	0	50	2	2	-0.159	0.161	0.957	0.020	150
1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 tone-sided rule one-sided rule tone-sided rule <t< td=""><td>1</td><td>50</td><td>2</td><td>0</td><td>0.721</td><td>1.273</td><td>0.939</td><td>0.023</td><td>50</td></t<>	1	50	2	0	0.721	1.273	0.939	0.023	50
1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 one-sided rule one-sided rule -1 50 2 0 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150	1	50	2	0.25	0.721	1.273	0.939	0.023	50
1 50 2 1 0.841 1.161 0.957 0.020 150 tone-sided rule cone-sided rule -1 50 2 0 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105	1	50	2	0.50	0.721	1.273	0.939	0.023	50
1 50 2 2 0.841 1.161 0.957 0.020 150 cone-sided rule -1 50 2 0 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 2 0 -0.172 0.249 0.947 0.176 105 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	1	50	2	0.75	0.731	1.276	0.955	0.026	52
one-sided rule -1 50 2 0 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150	1	50	2	1	0.841	1.161	0.957	0.020	150
-1 50 2 0 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.1	1	50	2	2	0.841	1.161	0.957	0.020	150
-1 50 2 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.16					C	ne-sided rul	e		
-1 50 2 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 1 50 2 2 -0.159 0.161 <td>-1</td> <td>50</td> <td>2</td> <td>0</td> <td>-1.159</td> <td>-0.839</td> <td>0.957</td> <td>0.020</td> <td>150</td>	-1	50	2	0	-1.159	-0.839	0.957	0.020	150
-1 50 2 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 1 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273	-1	50	2	0.25	-1.159	-0.839	0.957	0.020	150
-1 50 2 1 -1.159 -0.839 0.957 0.020 150 -1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 <	-1	50	2	0.50	-1.159	-0.839	0.957	0.020	150
-1 50 2 2 -1.159 -0.839 0.957 0.020 150 0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 <	-1	50	2	0.75	-1.159	-0.839	0.957	0.020	150
0 50 2 0 -0.172 0.249 0.947 0.176 105 0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 <t< td=""><td>-1</td><td>50</td><td>2</td><td>1</td><td>-1.159</td><td>-0.839</td><td>0.957</td><td>0.020</td><td>150</td></t<>	-1	50	2	1	-1.159	-0.839	0.957	0.020	150
0 50 2 0.25 -0.158 0.221 0.943 0.130 122 0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.	-1	50	2	2	-1.159	-0.839	0.957	0.020	150
0 50 2 0.50 -0.157 0.169 0.936 0.020 147 0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	0	-0.172	0.249	0.947	0.176	105
0 50 2 0.75 -0.159 0.161 0.957 0.020 150 0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	0.25	-0.158	0.221	0.943	0.130	122
0 50 2 1 -0.159 0.161 0.957 0.020 150 0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	0.50	-0.157	0.169	0.936	0.020	147
0 50 2 2 -0.159 0.161 0.957 0.020 150 1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	0.75	-0.159	0.161	0.957	0.020	150
1 50 2 0 0.721 1.273 0.939 0.023 50 1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	1	-0.159	0.161	0.957	0.020	150
1 50 2 0.25 0.721 1.273 0.939 0.023 50 1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	0	50	2	2	-0.159	0.161	0.957	0.020	150
1 50 2 0.50 0.721 1.273 0.939 0.023 50 1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	1	50	2	0	0.721	1.273	0.939	0.023	50
1 50 2 0.75 0.731 1.276 0.955 0.026 52 1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	1	50	2	0.25	0.721	1.273	0.939	0.023	50
1 50 2 1 0.841 1.161 0.957 0.020 150 1 50 2 2 0.841 1.161 0.957 0.020 150	1	50	2	0.50	0.721	1.273	0.939	0.023	50
1 50 2 2 0.841 1.161 0.957 0.020 150	1	50	2	0.75	0.731	1.276	0.955	0.026	52
	1	50	2	1	0.841	1.161	0.957	0.020	150
two-sided rule	1	50	2	2	0.841	1.161	0.957	0.020	150
					t	wo-sided rul	e		

Table 2 – *Continued from previous page*

μ n C γ Lower CL Upper CL Cov. Prob. Kol. Dist. Aver. Size				-	Table 2 – Cor				
-1 100 2 0.25 -1.196 -0.805 0.955 0.018 100 -1 100 2 0.50 -1.196 -0.805 0.955 0.018 100 -1 100 2 0.75 -1.196 -0.805 0.955 0.018 100 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.55 -0.113 0.113 0.954 0.020 300 0 100 2 0.50 -0.117 0.116 0.999 0.019 291 1 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 0.50 -0.117 0.116 0.991 0.019 291 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.111 0.118 0.940 0.019 296 0 100 2 0.75 0.113 0.113 0.954 0.020 300 0 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195 0.955 0.018 100 -1 100	μ	n	C	γ		Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size
-1 100 2 0.50 -1.196 -0.805 0.955 0.018 100 -1 100 2 0.75 -1.1196 -0.805 0.955 0.018 100 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.887 1.113 0.954 0.020 300 -1 100 2 0.887 1.113 0.954 0.020 300 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195 0.955 0.018 300 -1 100 2 0.50 0.804 1.195 0.955 0.018 300 -1 100 2 0.75 0.804 1.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.25 0.804 3.195 0.954 0.020 300 -1 100 2 0.25 0.113 0.887 0.954 0.020 300 -1 100 2 0.25 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.188 0.961 0.183 204 -1 100 2 0.75 0.113 0.178 0.961 0.183 204 -1 100 2 0.75 0.113 0.113 0.954 0.020 300 -1 100 2 0.75 0.113 0.113 0.954 0.020 300 -1 100 2 0.75 0.014 0.160 0.957 0.147 237 0 100 2 0.75 0.887 1.113 0.954 0.020 300 -1 100 2 0.75 0.887 1.113 0.954 0.020 300 -1 100 2 0.75 0.887 1.195 0.955 0.018 100 -1 100 2 0.75 0.887 1.195 0.955 0.018 100 -1 100 2 0.75 0.887 0.994 0.955 0.018 100 -1 100 2 0.75 0.887 0.994 0.955 0.018 100 -1 100 2 0.75 0.887 0.994 0.955 0.018 100 -1 100 2 0.75 0.887 0.994 0.9955 0.018 100 -1 100 2 0.75 0.887 0.994 0.9955 0.018 100 -1 100 2 0.75 0.887 0.994 0.9955 0.018 100 -1 100 2 0.75 0.887 0.994 0.9955 0.018 100 -1 100 2	-1					-0.805			100
-1 100 2 0.75 -1.196 -0.805 0.955 0.018 100 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 -1 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 0.00 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 1.113 0.954 0.020 300 -1 100 2 0.75 0.804 1.95 0.955 0.018 100 1 100 2 0.50 0.804 1.95 0.955 0.018 300 -1 100 2 0.75 0.804 1.95 0.955 0.018 300 -1 100 2 0.75 0.804 1.95 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.75 0.804 3.195 0.955 0.018 300 -1 100 2 0.50 0.887 0.113 0.954 0.020 300 -1 100 2 0.25 0.887 0.113 0.954 0.020 300 -1 100 2 0.25 0.1113 0.887 0.954 0.020 300 -1 100 2 0.25 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.50 0.1113 0.887 0.954 0.020 300 -1 100 2 0.75 0.1113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.75 0.113 0.887 0.954 0.020 300 -1 100 2 0.50 0.111 0.118 0.940 0.020 300 -1 100 2 0.25 0.114 0.160 0.957 0.147 237 0 100 2 0.25 0.114 0.160 0.957 0.147 237 0 100 2 0.50 0.111 0.118 0.940 0.020 300 0 100 2 1 0.013 0.113 0.954 0.020 300 1 100 2 0.75 0.113 0.113 0.954 0.020 300 1 100 2 0.887 1.113 0.954 0.020 300 1 100 2 0.8887 1.113 0.954 0.020 300 -1 100 2 0.50 0.114 0.118 0.940 0.020 300 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.50 0.804 1.195 0.955 0.018 100 -1 100 2 0.75 0.804 1.195	-1								
-1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 1 100 2 2 -0.113 0.113 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.804 1.195 0.955 0.018 100 1 100 2 0.804 1.195 0.955 0.018 200 1 100 2 0.50 0.804 1.195 0.955 0.018 200 1 100 2 0.50 0.804 1.195 0.955 0.018 200 1 100 2 0.50 0.804 1.195 0.955 0.018 200 1 100 2 0.50 0.804 1.195 0.955 0.018 200 1 100 2 0.50 0.804 2.195 0.955 0.018 200 1 100 2 0.75 0.804 2.195 0.955 0.018 200 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 0.954 0.020 300 1 100 2 1 0.887 0.954 0.020 300 1 100 2 0.50 0.887 0.9887 0.954 0.020 300 1 100 2 0.50 0.113 0.887 0.954 0.020 300 1 100 2 0.50 0.113 0.887 0.954 0.020 300 1 100 2 0.50 0.113 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 1 00 2 0.75 0.113 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.9887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.9887 0.954 0.020 300 1 1 00 2 0.50 0.011 0.118 0.940 0.020 300 1 1 00 2 0.50 0.011 0.118 0.940 0.020 300 1 1 00 2 0.50 0.011 0.118 0.940 0.020 300 1 1 00 2 0.50 0.011 0.118 0.940 0.020 300 1 1 00 2 0.50 0.011 0.118 0.954 0.020 300 1 1 00 2 0.50 0.804 1.195 0.955 0.018 100 1 1 100 2 0.887 1.113 0.954 0.020 300 1 1 100 2 0.887 1.113 0.954 0.020 300 1 1 100 2 0.887 1.113 0.954 0.020 300 1 1 100 2 0.887 1.113 0.954 0.020 300 1 1 100 2 0.887 0.912 0.957 0.020 300 1 1 100 2 0.887 0.912 0.957 0.020 300 1 1 100 2 0.050 0.804 1.195 0.955 0.018 100 1 1 100 2 0.500 0.804 1.195 0.955 0.018 100 1 1 100 2 0.500 0.804 1.195 0.955 0.018 100 1 1 100 2 0.500 0.804 1.195 0.955 0.018 100 1 1 100 2 0.500 0.804 1.195 0.955 0.018 100 1 1 100 2 0.0500 0.0	-1	100		0.50	-1.196	-0.805	0.955	0.018	100
-1 100 2 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 1 00 2 2 -0.113 0.113 0.954 0.020 300 1 00 2 2 -0.113 0.113 0.954 0.020 300 1 00 2 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 00 2 0.50 0.887 1.113 0.954 0.020 300 1 1 00 2 0.50 0.887 1.113 0.955 0.918 100 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 00 2 1 0.887 1.113 0.954 0.020 300 1 1 00 2 1 0.887 1.113 0.954 0.020 300 1 1 00 2 1 0.887 0.955 0.018 100 1 100 2 1 0.887 0.955 0.018 100 1 100 2 1 0.887 0.955 0.018 100 1 100 2 1 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 00 2 0 0.50 0.113 0.887 0.954 0.020 300 1 00 2 0.50 0.113 0.887 0.954 0.020 300 1 00 2 0 0.50 0.113 0.887 0.954 0.020 300 1 00 2 0 0.050 0.113 0.887 0.954 0.020 300 1 00 2 0 0.020 0.113 0.188 0.961 0.183 204 0.100 2 0 0.25 0.113 0.188 0.961 0.183 204 0.100 2 0.25 0.114 0.160 0.957 0.147 237 0.100 2 0.25 0.114 0.160 0.957 0.147 237 0.100 2 0.25 0.114 0.160 0.957 0.147 237 0.100 2 0.25 0.114 0.160 0.957 0.147 237 0.100 2 0.50 0.111 0.118 0.944 0.020 300 0.100 2 0.25 0.114 0.160 0.957 0.147 237 0.100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.887 1.113 0.113 0.954 0.020 300 0.100 2 0.050 0.111 0.118 0.945 0.020 300 1 00 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 100 2 0.50 0.887 1.113 0.113 0.954 0.020 300 0.100 2 0.050 0.887 1.113 0.954 0.020 300 0.100 2 0.050 0.887 1.113 0.954 0.020 300 0.100 2 0.50 0.887 1.113 0.955 0.018 100 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 100 2 0.50 0.887 1.113 0.954 0.020 300 1 1 100 2 0.50 0.50 0.887 1.113 0.954 0.020 300 1	-1	100			-1.196	-0.805	0.955	0.018	
0 100 2 0 -0.186 0.185 0.955 0.073 120 0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.887 1.113 <td>-1</td> <td>100</td> <td></td> <td></td> <td>-1.113</td> <td>-0.887</td> <td>0.954</td> <td>0.020</td> <td>300</td>	-1	100			-1.113	-0.887	0.954	0.020	300
0 100 2 0.25 -0.163 0.160 0.948 0.142 175 0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 1 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 1.113 -0.887	-1	100			-1.113	-0.887	0.954	0.020	300
0 100 2 0.50 -0.117 0.116 0.919 0.019 291 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 1.113 0.887	0			0		0.185	0.955	0.073	120
0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.50 -1.113 -0.8					-0.163				
0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.55 -1.113 -0.887 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.88	0			0.75		0.113			
1 100	0								
1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 -1 100 2 0 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113							0.954		
1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 cone-sided rule -1 100 2 0 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 0 100									
1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 one-sided rule -1 100 2 0 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1.113 -0.887 0.954 0.020 300 -1 100 2 0123 0.178 0.954 0.020 300 0 100 2 0.25									
1 100 2 1 0.887 1.113 0.954 0.020 300 one-sided rule -1 100 2 0 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.012 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 0 -0.123 0.178 0.954 0.020 300 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100									
1 100 2 2 0.887 1.113 0.954 0.020 300									
One-sided rule									
-1 100 2 0 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.25 -1.113 -0.887 0.954 0.012 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 1 -0.113	_1	100	2	2				0.020	300
-1 100 2 0.25 -1.113 -0.887 0.954 0.012 300 -1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 500 2 0.75 0.807 0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.087 -0.912 0.957 0.020 500									
-1 100 2 0.50 -1.113 -0.887 0.954 0.020 300 -1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 500 2 0.75 0.804 0.020 300 1 100 2 1 0.887 0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500									
-1 100 2 0.75 -1.113 -0.887 0.954 0.020 300 -1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 500 2 0.75 0.804 0.095 0.955 0.018 0.000 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 100 2 1 -1.113 -0.887 0.954 0.020 300 -1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
-1 100 2 2 -1.113 -0.887 0.954 0.020 300 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0 804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 1500 -1.050 -0.949 0.953 0.024 15									
0 100 2 0 -0.123 0.178 0.961 0.183 204 0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
0 100 2 0.25 -0.114 0.160 0.957 0.147 237 0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
0 100 2 0.50 -0.111 0.118 0.940 0.019 296 0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 1.113									
0 100 2 0.75 -0.113 0.113 0.954 0.020 300 0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 1 0.887 1.113 0.954 0.020 300 -1 500 2 0.25 -1.087 -0.912									
0 100 2 1 -0.113 0.113 0.954 0.020 300 0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 -1 500 2 0.25 -1.087 -0.912									
0 100 2 2 -0.113 0.113 0.954 0.020 300 1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.55 -1.087 -0.912									
1 100 2 0 0.804 1.195 0.955 0.018 100 1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 two-sided rule -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1									
1 100 2 0.25 0.804 1.195 0.955 0.018 100 1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 1 100 2 2 0.887 1.113 0.954 0.020 300 1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1									
1 100 2 0.50 0.804 1.195 0.955 0.018 100 1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 two-sided rule -1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500									
1 100 2 0.75 0.804 1.195 0.955 0.018 100 1 100 2 1 0.887 1.113 0.954 0.020 300 two-sided rule -1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
1 100 2 1 0.887 1.113 0.954 0.020 300 two-sided rule -1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
1 100 2 2 0 0.887 1.113 0.954 0.020 300 two-sided rule -1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
two-sided rule -1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 500 2 0 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500	1	100	2	2				0.020	300
-1 500 2 0.25 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 500 2 0.50 -1.087 -0.912 0.957 0.020 500 -1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 500 2 0.75 -1.087 -0.912 0.957 0.020 500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
-1 500 2 2 -1.050 -0.949 0.953 0.024 1500									
	-1	500	2	2	-1.050	-0.949			

Table 2 – *Continued from previous page*

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
0 500 2 0.25 -0.077 0.079 0.953 0.134 719 0 500 2 0.50 -0.052 0.053 0.901 0.030 1440 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.
0 500 2 0.50 -0.052 0.053 0.901 0.030 1440 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.0
0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 1.051 0.953 0.024 1500 -1 500 2 0 -1.050 -0.949 0.95
0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1.050 1.051 0.953 0.024 1500 1 500 2 1.050 1.051 0.953 0.024 1500 1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 1 500 2 0.550 -1.050 -0.949 0.953
0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 1 0.950 1.051 0.953 0.024 1500 -1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.55 -1.050 -0.
1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 <t< td=""></t<>
1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 -1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050
1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 one-sided rule -1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 0 500
1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 one-sided rule one-sided rule -1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500
1 500 2 1 0.950 1.051 0.953 0.024 1500 two-sided rule one-sided rule one-sided rule -1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082
1 500 2 2 0.950 1.051 0.953 0.024 1500
One-sided rule
-1 500 2 0 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500
-1 500 2 0.25 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500
-1 500 2 0.50 -1.050 -0.949 0.953 0.024 1500 -1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500
-1 500 2 0.75 -1.050 -0.949 0.953 0.024 1500 -1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.75 0.913 1.081 0.953 0.024 1500
-1 500 2 1 -1.050 -0.949 0.953 0.024 1500 -1 500 2 2 -1.050 -0.949 0.953 0.024 1500 0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500
-1 500 2 2
0 500 2 0 -0.057 0.082 0.963 0.194 963 0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.08
0 500 2 0.25 -0.052 0.078 0.961 0.201 1083 0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.05
0 500 2 0.50 -0.049 0.054 0.927 0.030 1469 0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051
0 500 2 0.75 -0.050 0.051 0.953 0.024 1500 0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051
0 500 2 1 -0.050 0.051 0.953 0.024 1500 0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
0 500 2 2 -0.050 0.051 0.953 0.024 1500 1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 0 0.913 1.088 0.957 0.020 500 1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 0.25 0.913 1.088 0.957 0.020 500 1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 0.50 0.913 1.088 0.957 0.020 500 1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 0.75 0.913 1.088 0.957 0.020 500 1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 1 0.950 1.051 0.953 0.024 1500 1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
1 500 2 2 0.950 1.051 0.953 0.024 1500 two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
two-sided rule -1 10 1 0 -1.600 -0.401 0.912 0.019 10
-1 10 1 0 -1.600 -0.401 0.912 0.019 10
-1 10 1 0.25 -1.601 -0.402 0.913 0.019 10
-1 10 1 0.50 -1.603 -0.406 0.918 0.019 10
-1 10 1 0.75 -1.610 -0.439 0.929 0.041 11
-1 10 1 1 -1.575 -0.601 0.926 0.184 19
-1 10 1 2 -1.357 -0.647 0.939 0.018 30
0 10 1 0 -0.553 0.556 0.910 0.106 13
0 10 1 0.25 -0.509 0.515 0.907 0.142 16
0 10 1 0.50 -0.448 0.441 0.897 0.128 22
0 10 1 0.75 -0.379 0.369 0.887 0.042 28
0 10 1 1 -0.357 0.355 0.937 0.018 30
0 10 1 2 -0.357 0.353 0.939 0.018 30

Table 2 – *Continued from previous page*

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
1 10 1 0.25 0.405 1.604 0.914 0.019 1 10 1 0.50 0.410 1.606 0.919 0.019 1 10 1 0.75 0.443 1.617 0.940 0.044 1 10 1 1 0.602 1.576 0.928 0.176 1 10 1 2 0.643 1.353 0.939 0.018 -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357
1 10 1 0.50 0.410 1.606 0.919 0.019 1 10 1 0.75 0.443 1.617 0.940 0.044 1 10 1 1 0.602 1.576 0.928 0.176 1 10 1 2 0.643 1.353 0.939 0.018 -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357
1 10 1 0.75 0.443 1.617 0.940 0.044 1 10 1 1 0.602 1.576 0.928 0.176 1 10 1 2 0.643 1.353 0.939 0.018 -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 0 -0.370
1 10 1 1 0.602 1.576 0.928 0.176 1 10 1 2 0.643 1.353 0.939 0.018 one-sided rule -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
1 10 1 2 0.643 1.353 0.939 0.018 one-sided rule -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 0 -0.370 0.547 0.927 0.178 0 10 1
one-sided rule -1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 0 0 0.370 0.547 0.939 0.018 0 10 1 0 0.25 -0.353 0.518 0.924 0.165
-1 10 1 0 -1.357 -0.646 0.938 0.018 -1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
-1 10 1 0.25 -1.357 -0.646 0.938 0.018 -1 10 1 0.50 -1.357 -0.647 0.939 0.018 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
-1 10 1 0.50 -1.357 -0.647 0.939 0.018 3 -1 10 1 0.75 -1.357 -0.647 0.939 0.018 3 -1 10 1 1 -1.357 -0.647 0.939 0.018 3 -1 10 1 2 -1.357 -0.647 0.939 0.018 3 0 10 1 0 -0.370 0.547 0.927 0.178 3 0 10 1 0.25 -0.353 0.518 0.924 0.165 3
-1 10 1 0.75 -1.357 -0.647 0.939 0.018 -1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
-1 10 1 1 -1.357 -0.647 0.939 0.018 -1 10 1 2 -1.357 -0.647 0.939 0.018 0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
-1 10 1 2 -1.357 -0.647 0.939 0.018 0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
0 10 1 0 -0.370 0.547 0.927 0.178 0 10 1 0.25 -0.353 0.518 0.924 0.165
0 10 1 0.25 -0.353 0.518 0.924 0.165
0 10 1 0.50 -0.340 0.456 0.919 0.115
0 10 1 0.75 -0.347 0.3812 0.916 0.031
0 10 1 1 -0.356 0.355 0.937 0.018
0 10 1 2 -0.3571 0.353 0.939 0.018
1 10 1 0 0.403 1.602 0.912 0.019
1 10 1 0.25 0.405 1.604 0.914 0.019
1 10 1 0.50 0.410 1.606 0.919 0.019
1 10 1 0.75 0.443 1.617 0.940 0.044
1 10 1 1 0.602 1.576 0.928 0.176
1 10 1 2 0.643 1.353 0.939 0.018
two-sided rule
-1 50 1 0 -1.279 -0.727 0.939 0.023
-1 50 1 0.25 -1.279 -0.727 0.939 0.023 5
-1 50 1 0.50 -1.279 -0.727 0.939 0.023
-1 50 1 0.75 -1.279 -0.727 0.939 0.023 5
-1 50 1 1 -1.266 -0.819 0.949 0.190
-1 50 1 2 -1.159 -0.839 0.957 0.020 15
0 50 1 0 -0.272 0.263 0.938 0.075
0 50 1 0.25 -0.255 0.247 0.935 0.135
0 50 1 0.50 -0.205 0.201 0.926 0.126 1
0 50 1 0.75 -0.161 0.161 0.948 0.020 14
0 50 1 1 -0.159 0.161 0.957 0.020 15
0 50 1 2 -0.159 0.161 0.957 0.020 15
1 50 1 0 0.721 1.273 0.939 0.023
1 50 1 0.25 0.721 1.273 0.939 0.023
1 50 1 0.50 0.721 1.273 0.939 0.023
1 50 1 0.75 0.721 1.273 0.939 0.023
1 50 1 1 0.819 1.261 0.948 0.187
<u>1 50 1 2 0.841 1.161 0.957 0.020 15</u>

Table 2 – *Continued from previous page*

				Table 2 – Con							
μ	n	C	γ	Lower CL	Upper CL		Kol.Dist.	Aver.Size			
one-sided rule											
-1	50	1	0	-1.159	-0.839	0.957	0.020	150			
-1	50	1	0.25	-1.159	-0.839	0.957	0.020	150			
-1	50	1	0.50	-1.159	-0.839	0.957	0.020	150			
-1	50	1	0.75	-1.159	-0.839	0.957	0.020	150			
-1	50	1	1	-1.159	-0.839	0.957	0.020	150			
-1	50	1	2	-1.159	-0.839	0.957	0.020	150			
0	50	1	0	-0.177	0.255	0.947	0.183	100			
0	50	1	0.25	-0.168	0.243	0.946	0.158	109			
0	50	1	0.50	-0.155	0.208	0.942	0.126	130			
0	50	1	0.75	-0.158	0.162	0.953	0.020	150			
0	50	1	1	-0.159	0.161	0.957	0.020	150			
0	50	1	2	-0.159	0.161	0.957	0.020	150			
1	50	1	0	0.721	1.273	0.939	0.023	50			
1	50	1	0.25	0.721	1.273	0.939	0.023	50			
1	50	1	0.50	0.721	1.273	0.939	0.023	50			
1	50	1	0.75	0.721	1.273	0.939	0.023	50			
1	50	1	1	0.819	1.261	0.948	0.187	95			
1	50	1	2	0.841	1.161	0.957	0.020	150			
					wo-sided rul	e					
-1	100	1	0	-1.196	-0.805	0.955	0.018	100			
-1	100	1	0.25	-1.196	-0.805	0.955	0.018	100			
-1	100	1	0.50	-1.196	-0.805	0.955	0.018	100			
-1	100	1	0.75	-1.196	-0.805	0.955	0.018	100			
-1	100	1	1	-1.185	-0.869	0.949	0.184	187			
-1	100	1	2	-1.113	-0.887	0.954	0.020	300			
0	100	1	0	-0.191	0.190	0.955	0.041	109			
0	100	1	0.25	-0.179	0.178	0.955	0.111	135			
0	100	1	0.50	-0.141	0.143	0.939	0.118	225			
0	100	1	0.75	-0.113	0.113	0.954	0.020	300			
0	100	1	1	-0.113	0.113	0.954	0.020	300			
0	100	1	2	-0.113	0.113	0.954	0.020	300			
1	100	1	0	0.804	1.195	0.955	0.018	100			
1	100	1	0.25	0.804	1.195	0.955	0.018	100			
1	100	1	0.50	0.804	1.195	0.955	0.018	100			
1	100	1	0.75	0.804	1.195	0.955	0.018	100			
1	100	1	1	0.871	1.184	0.963	0.188	189			
1	100	1	2	0.887	1.113	0.954	0.020	300			
				C	ne-sided rule	e					
-1	100	1	0	-1.113	-0.887	0.954	0.020	300			
-1	100	1	0.25	-1.113	-0.887	0.954	0.020	300			
-1	100	1	0.50	-1.113	-0.887	0.954	0.020	300			
-1	100	1	0.75	-1.113	-0.887	0.954	0.020	300			
-1	100	1	1	-1.113	-0.887	0.954	0.020	300			
						-	Continued of				

Table 2 – *Continued from previous page*

	Table 2 – Continued from previous page									
μ	n	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size		
-1	100	1	2	-1.113	-0.887	0.954	0.020	300		
0	100	1	0	-0.126	0.181	0.961	0.184	196		
0	100	1	0.25	-0.120	0.173	0.960	0.178	213		
0	100	1	0.50	-0.109	0.145	0.951	0.109	263		
0	100	1	0.75	-0.113	0.114	0.954	0.020	300		
0	100	1	1	-0.113	0.113	0.954	0.020	300		
0	100	1	2	-0.113	0.113	0.954	0.020	300		
1	100	1	0	0.804	1.195	0.955	0.018	100		
1	100	1	0.25	0.804	1.195	0.955	0.018	100		
1	100	1	0.50	0.804	1.195	0.955	0.018	100		
1	100	1	0.75	0.804	1.195	0.955	0.018	100		
1	100	1	1	0.871	1.184	0.963	0.188	189		
1	100	1	2	0.887	1.113	0.954	0.020	300		
					wo-sided rul	e				
-1	500	1	0	-1.087	-0.912	0.957	0.020	500		
-1	500	1	0.25	-1.087	-0.912	0.957	0.020	500		
-1	500	1	0.50	-1.087	-0.912	0.957	0.020	500		
-1	500	1	0.75	-1.087	-0.912	0.957	0.020	500		
-1	500	1	1	-1.082	-0.941	0.949	0.187	945		
-1	500	1	2	-1.050	-0.949	0.953	0.024	1500		
0	500	1	0	-0.086	0.087	0.957	0.035	519		
0	500	1	0.25	-0.082	0.084	0.956	0.090	596		
0	500	1	0.50	-0.063	0.064	0.940	0.126	1120		
0	500	1	0.75	-0.050	0.051	0.953	0.024	1500		
0	500	1	1	-0.050	0.051	0.953	0.024	1500		
0	500	1	2	-0.050	0.051	0.953	0.024	1500		
1	500	1	0	0.913	1.088	0.957	0.020	500		
1	500	1	0.25	0.913	1.088	0.957	0.020	500		
1	500	1	0.50	0.913	1.088	0.957	0.020	500		
1	500	1	0.75	0.913	1.088	0.957	0.020	500		
1	500	1	1	0.942	1.083	0.964	0.186	936		
_1	500	1	2	0.950	1.051	0.953	0.024	1500		
				(one-sided rule	e				
-1	500	1	0	-1.050	-0.949	0.953	0.024	1500		
-1	500	1	0.25	-1.050	-0.949	0.953	0.024	1500		
-1	500	1	0.50	-1.050	-0.949	0.953	0.024	1500		
-1	500	1	0.75	-1.0503	-0.949	0.953	0.024	1500		
-1	500	1	1	-1.050	-0.949	0.953	0.024	1500		
-1	500	1	2	-1.050	-0.949	0.953	0.024	1500		
0	500	1	0	-0.057	0.083	0.963	0.189	949		
0	500	1	0.25	-0.055	0.081	0.962	0.207	1004		
0	500	1	0.50	-0.049	0.066	0.953	0.128	1305		
0	500	1	0.75	-0.050	0.051	0.953	0.024	1500		
0	500	1	1	-0.050	0.051	0.953	0.024	1500		
							7			

Table 2 – *Continued from previous page*

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				-	Table 2 – <i>Con</i>	tinued from p	previous pag	e	_
1 500	μ	n	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size
1 500	0	500	1	2	-0.050	0.051	0.953	0.024	1500
1 500	1	500	1	0	0.913	1.088	0.957	0.020	500
1 500	1	500	1	0.25	0.913	1.088	0.957	0.020	500
1 500	1	500	1	0.50	0.913	1.088	0.957	0.020	500
1 500	1	500	1	0.75	0.913	1.088	0.957	0.020	500
One-sided rule	1	500	1	1	0.942	1.083	0.964	0.186	936
-1 10 0 0 0 -1.356	1	500	1	2	0.950	1.051	0.953	0.024	1500
-1 10 0 0 0.25					C	ne-sided rule	2		
-1 10 0 0 0.50 -1.356 -0.645 0.937 0.018 30 -1 10 0 0 0.75 -1.356 -0.645 0.937 0.018 30 -1 10 0 1 -1.356 -0.645 0.937 0.018 30 -1 10 0 2 -1.356 -0.645 0.937 0.018 30 -1 10 0 0 2 -1.356 -0.645 0.937 0.018 30 -1 10 0 0 0 -0.398 0.576 0.928 0.176 19 0 10 0 0.25 -0.398 0.576 0.928 0.176 19 0 10 0 0.50 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.55 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 0 1 -0.398 0.576 0.928 0.176 19 1 10 0 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0 0.402 1.602 0.911 0.019 10 1 10 0 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0 0.55 0.402 1.602 0.911 0.019 10 1 10 0 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 0 0.55 0.402 1.602 0.911 0.019 10 1 10 0 0 0.55 0.402 1.602 0.911 0.019 10 1 10 0 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 0 0.50 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0 0.50 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0 0.50 0.50 0.50 0.50 0.50 0.50 0	-1	10	0	0	-1.356	-0.645	0.937	0.018	30
-1 10 0 0 0.75 -1.356 -0.645 0.937 0.018 30 -1 10 0 1 -1.356 -0.645 0.937 0.018 30 -1 10 0 2 -1.356 -0.645 0.937 0.018 30 0 10 0 0 0 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.25 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0 1 0.402 1.602 0.911 0.019 10 1 10 0 0 2 0.402 1.602 0.911 0.019 10 1 10 0 0 2 0.402 1.602 0.911 0.019 10 1 10 0 0 1 0.402 1.602 0.911 0.019 10 1 10 0 0 1 0.402 1.602 0.911 0.019 10 1 10 0 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.0000 0.0000 0.0000 0.00000 0.00000	-1	10	0	0.25	-1.356	-0.645	0.937	0.018	30
-1 10 0 1 -1.356	-1	10	0	0.50	-1.356	-0.645	0.937	0.018	30
-1 10 0 2 -1.356 -0.645 0.937 0.018 30 0 10 0 0 0 -0.398 0.576 0.928 0.176 19 0 10 0 0.25 -0.398 0.576 0.928 0.176 19 0 10 0 0.50 -0.398 0.576 0.928 0.176 19 0 10 0 0.55 -0.398 0.576 0.928 0.176 19 0 10 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 2 -0.398 0.576 0.928 0.176 19 0 10 0 2 -0.398 0.576 0.928 0.176 19 10 0 10 0 2 -0.398 0.576 0.928 0.176 19 10 0 10 0 0 2 -0.398 0.576 0.928 0.176 19 10 10 0 0 2 0.402 1.602 0.911 0.019 10 10 10 0 0.25 0.402 1.602 0.911 0.019 10 10 10 0 0.50 0.402 1.602 0.911 0.019 10 10 10 0 0.50 0.402 1.602 0.911 0.019 10 10 10 0 0.75 0.402 1.602 0.911 0.019 10 10 10 0 0.75 0.402 1.602 0.911 0.019 10 10 10 0 0.75 0.402 1.602 0.911 0.019 10 10 10 0 0.50 0.402 1.602 0.911 0.019 10 10 10 10 0 0.50 0.402 1.602 0.911 0.019 10 10 10 10 0 0.50 0.402 1.602 0.911 0.019 10 10 10 10 10 10 10 10 10	-1	10	0	0.75	-1.356	-0.645	0.937	0.018	30
0 10 0 0 -0.398 0.576 0.928 0.176 19 0 10 0 0.25 -0.398 0.576 0.928 0.176 19 0 10 0 0.50 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 1 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 <td>-1</td> <td>10</td> <td>0</td> <td>1</td> <td>-1.356</td> <td>-0.645</td> <td>0.937</td> <td>0.018</td> <td>30</td>	-1	10	0	1	-1.356	-0.645	0.937	0.018	30
0 10 0 0.25 -0.398 0.576 0.928 0.176 19 0 10 0 0.50 -0.398 0.576 0.928 0.176 19 0 10 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 1 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0.402 1.602 0.911 0.019 10 1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 1.50 1.602 0.911 0.019 10 1 10 0 1.602 0.911 0.019 10 <t< td=""><td>-1</td><td>10</td><td>0</td><td>2</td><td>-1.356</td><td>-0.645</td><td>0.937</td><td>0.018</td><td>30</td></t<>	-1	10	0	2	-1.356	-0.645	0.937	0.018	30
0 10 0 0.50 -0.398 0.576 0.928 0.176 19 0 10 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 1 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0.402 1.602 0.911 0.019 10 1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 1.075 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 <td>0</td> <td>10</td> <td>0</td> <td>0</td> <td>-0.398</td> <td>0.576</td> <td>0.928</td> <td>0.176</td> <td>19</td>	0	10	0	0	-0.398	0.576	0.928	0.176	19
0 10 0 0.75 -0.398 0.576 0.928 0.176 19 0 10 0 1 -0.398 0.576 0.928 0.176 19 0 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0.402 1.602 0.911 0.019 10 1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911	0	10	0	0.25	-0.398	0.576	0.928	0.176	19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	10	0	0.50	-0.398	0.576	0.928	0.176	19
0 10 0 2 -0.398 0.576 0.928 0.176 19 1 10 0 0 0.402 1.602 0.911 0.019 10 1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 1.075 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 10 0 2 0.402 1.602 0.911 0.019 10 1 50 0 0 0.25 -1.159 -0.839	0	10	0	0.75	-0.398	0.576	0.928	0.176	19
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0	10	0		-0.398	0.576	0.928	0.176	19
1 10 0 0.25 0.402 1.602 0.911 0.019 10 1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 To 0.402 1.502 0.911 0.019 10 0.019 150 -1 50 0 0.502 -1.159 -0.839 <td>0</td> <td>10</td> <td>0</td> <td>2</td> <td>-0.398</td> <td>0.576</td> <td>0.928</td> <td>0.176</td> <td>19</td>	0	10	0	2	-0.398	0.576	0.928	0.176	19
1 10 0 0.50 0.402 1.602 0.911 0.019 10 1 10 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 In the colspan="6">One-sided rule One-sided rule -1 50 0 0 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 <td>1</td> <td>10</td> <td>0</td> <td>0</td> <td>0.402</td> <td>1.602</td> <td>0.911</td> <td>0.019</td> <td>10</td>	1	10	0	0	0.402	1.602	0.911	0.019	10
1 10 0 0.75 0.402 1.602 0.911 0.019 10 1 10 0 1 0.402 1.602 0.911 0.019 10 tone-sided rule one-sided rule -1 50 0 0 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 <	1	10	0	0.25	0.402	1.602	0.911	0.019	10
1 10 0 1 0.402 1.602 0.911 0.019 10 cone-sided rule cone-sided rule -1 50 0 0 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 0 -0.181 0.261 0.948 0.187 95	1	10	0	0.50	0.402	1.602	0.911	0.019	10
1 10 0 2 0.402 1.602 0.911 0.019 10 one-sided rule -1 50 0 0 0 .25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 0 0 0 0 0 0 0 0 0 0.181 0.261 0.948 0.187 95 0 50 0 0 0.50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 0 1 0 0.75 -0.181 0.261	1	10	0	0.75	0.402	1.602	0.911	0.019	10
one-sided rule -1 50 0 0 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0	1	10	0	1	0.402	1.602	0.911	0.019	10
-1 50 0 0 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.	1	10	0	2	0.402	1.602	0.911	0.019	10
-1 50 0 0.25 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 <td></td> <td></td> <td></td> <td></td> <td>C</td> <td>ne-sided rule</td> <td>2</td> <td></td> <td></td>					C	ne-sided rule	2		
-1 50 0 0.50 -1.159 -0.839 0.957 0.020 150 -1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261	-1	50	0	0	-1.159	-0.839	0.957	0.020	150
-1 50 0 0.75 -1.159 -0.839 0.957 0.020 150 -1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 <t< td=""><td>-1</td><td>50</td><td>0</td><td>0.25</td><td>-1.159</td><td>-0.839</td><td>0.957</td><td>0.020</td><td>150</td></t<>	-1	50	0	0.25	-1.159	-0.839	0.957	0.020	150
-1 50 0 1 -1.159 -0.839 0.957 0.020 150 -1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.	-1	50	0	0.50	-1.159	-0.839	0.957	0.020	150
-1 50 0 2 -1.159 -0.839 0.957 0.020 150 0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.9	-1	50	0	0.75	-1.159	-0.839	0.957	0.020	150
0 50 0 0 -0.181 0.261 0.948 0.187 95 0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.93	-1	50	0	1	-1.159	-0.839	0.957	0.020	150
0 50 0 0.25 -0.181 0.261 0.948 0.187 95 0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.	-1	50	0	2	-1.159	-0.839	0.957	0.020	150
0 50 0 0.50 -0.181 0.261 0.948 0.187 95 0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	0	-0.181	0.261	0.948	0.187	95
0 50 0 0.75 -0.181 0.261 0.948 0.187 95 0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	0.25	-0.181	0.261	0.948	0.187	95
0 50 0 1 -0.181 0.261 0.948 0.187 95 0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	0.50	-0.181	0.261	0.948	0.187	95
0 50 0 2 -0.181 0.261 0.948 0.187 95 1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	0.75	-0.181	0.261	0.948	0.187	95
1 50 0 0 0.721 1.273 0.939 0.023 50 1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	1	-0.181	0.261	0.948	0.187	95
1 50 0 0.25 0.721 1.273 0.939 0.023 50 1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	0	50	0	2	-0.181	0.261	0.948	0.187	95
1 50 0 0.50 0.721 1.273 0.939 0.023 50 1 50 0 0.75 0.721 1.273 0.939 0.023 50	1	50	0	0	0.721	1.273	0.939	0.023	50
1 50 0 0.75 0.721 1.273 0.939 0.023 50	1	50	0	0.25	0.721	1.273	0.939	0.023	50
	1	50	0	0.50	0.721	1.273	0.939	0.023	50
<u>1 50 0 1 0.721 1.273 0.939 0.023</u> 50	1	50	0	0.75	0.721	1.273	0.939	0.023	50
	_1	50	0	1	0.721	1.273	0.939	0.023	50

Table 2 – *Continued from previous page*

	Table 2 – Continued from previous page										
μ	n	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size			
1	50	0	2	0.721	1.273	0.939	0.023	50			
					one-sided rule)					
-1	100	0	0	-1.113	-0.887	0.954	0.020	300			
-1	100	0	0.25	-1.113	-0.887	0.954	0.020	300			
-1	100	0	0.50	-1.113	-0.887	0.954	0.020	300			
-1	100	0	0.75	-1.113	-0.887	0.954	0.020	300			
-1	100	0	1	-1.113	-0.88	0.954	0.020	300			
-1	100	0	2	-1.113	-0.887	0.954	0.020	300			
0	100	0	0	-0.129	0.184	0.963	0.188	189			
0	100	0	0.25	-0.129	0.184	0.963	0.188	189			
0	100	0	0.50	-0.129	0.184	0.963	0.188	189			
0	100	0	0.75	-0.129	0.184	0.963	0.188	189			
0	100	0	1	-0.129	0.184	0.963	0.188	189			
0	100	0	2	-0.129	0.184	0.963	0.188	189			
1	100	0	0	0.804	1.195	0.955	0.011	100			
1	100	0	0.25	0.804	1.195	0.955	0.011	100			
1	100	0	0.50	0.804	1.195	0.955	0.018	100			
1	100	0	0.75	0.804	1.195	0.955	0.018	100			
1	100	0	1	0.804	1.195	0.955	0.018	100			
1	100	0	2	0.804	1.195	0.955	0.018	100			
	one-sided rule										
-1	500	0	0	-1.050	-0.949	0.953	0.024	1500			
-1	500	0	0.25	-1.050	-0.949	0.953	0.024	1500			
-1	500	0	0.50	-1.050	-0.949	0.953	0.024	1500			
-1	500	0	0.75	-1.050	-0.949	0.953	0.024	1500			
-1	500	0	1	-1.050	-0.949	0.953	0.024	1500			
-1	500	0	2	-1.050	-0.949	0.953	0.024	1500			
0	500	0	0	-0.058	0.083	0.964	0.186	936			
0	500	0	0.25	-0.058	0.083	0.964	0.186	936			
0	500	0	0.50	-0.058	0.083	0.964	0.186	936			
0	500	0	0.75	-0.058	0.083	0.964	0.186	936			
0	500	0	1	-0.058	0.083	0.964	0.186	936			
0	500	0	2	-0.058	0.083	0.964	0.186	936			
1	500	0	0	0.913	1.088	0.957	0.020	500			
1	500	0	0.25	0.913	1.088	0.957	0.020	500			
1	500	0	0.50	0.913	1.088	0.957	0.020	500			
1	500	0	0.75	0.913	1.088	0.957	0.020	500			
1	500	0	1	0.913	1.088	0.957	0.020	500			
1	500	0	2	0.913	1.088	0.957	0.020	500			
					two-sided rule	<u> </u>					
0	100	1	0.25	-0.179	0.178	0.955	0.111	135			
0	500	1	0.25	-0.082	0.084	0.956	0.090	596			
0	1000	1	0.25	-0.059	0.061	0.942	0.086	1137			
0	2000	1	0.25	-0.041	0.043	0.961	0.066	2312			
							<i>C</i>				

Table 2 – Continued from previous page

μ	n	C	γ	Lower CL	Upper CL	Cov.Prob.	Kol.Dist.	Aver.Size
two-sided rule								
0	100	2	0.25	-0.163	0.160	0.948	0.142	175
0	500	2	0.25	-0.077	0.079	0.953	0.134	719
0	1000	2	0.25	-0.056	0.058	0.940	0.119	1331
0	2000	2	0.25	-0.039	0.041	0.961	0.101	2666