

Optimal stiffness of longitudinal stiffeners in girders subjected to patch loading

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1. Introduction

I. BACKGROUND

- Hungarian bridges are built using an incremental launching method, causing a temporary patch loading condition
- Longitudinally stiffened girders are used to resist against patch loading

II. PROBLEM

- Design method for longitudinally stiffened girders in EN 1993-1-5 underestimates the patch loading resistance
- EN 1993-1-5 only handles girders with one longitudinal stiffener
- EN 1993-1-5 does not take different failure modes into account

III. GOAL

- Analyse the influence of different parameters on the patch loading resistance
- Proposal of new formulation for "strong" or "weak" longitudinal stiffeners

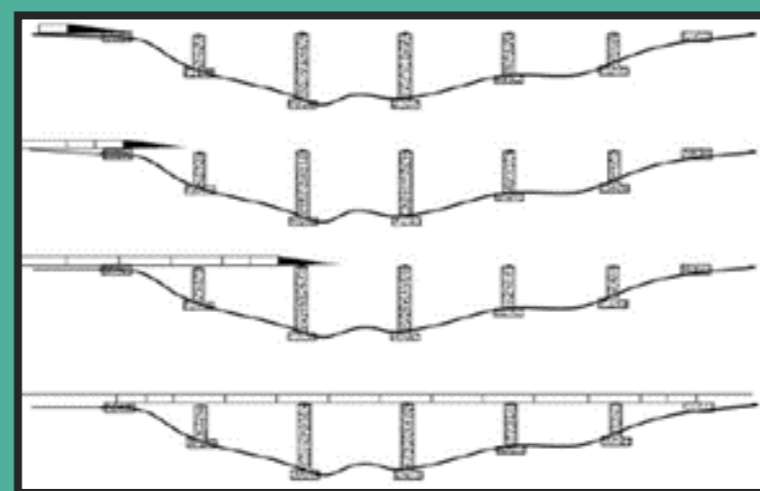


Figure 1: Incremental launching method [2, p.39]

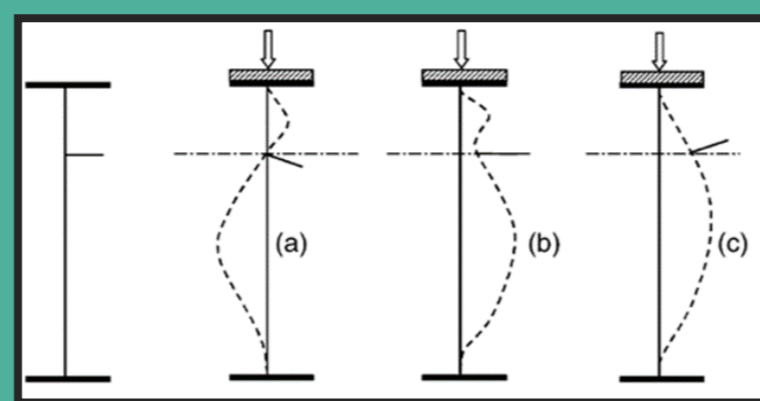


Figure 2: Failure modes, depending on the rigidity stiffness of the stiffener: a) local buckling, b) interaction of local and global buckling, c) global buckling [3, p. 564]



2. Method

I. Model development

- Longitudinally stiffened girder developed in ANSYS
- Geometrically and Materially Nonlinear Imperfection Analysis (GMNIA) and Linear Buckling Analysis (LBA)

II. Model validation

- Validated with experiments of Seitz.
- Manual imperfections (1 global imperfection, 3 local imperfections)
- Comparison numerical results vs. experimental results

III. Parameter identification

- Investigating the parameters given in the current EN 1993-1-5 formulation in function of the optimal stiffness
- Chosen parameters / ratio: loaded length (s_s), length (a), height (h_w), thickness web (t_w) and height loaded subpanel over thickness web (b_1/t_w)

$$\gamma_{s_opt_EC} = 13 \left(\frac{a}{h_w} \right)^3 + 210 \left(0,3 - \frac{b_1}{a} \right)$$

4. Conclusion

I. Parameters

- Loaded length: no influence
- Length of the girder: $1/a$ increasing influence
- Height of the web: $1/h_w$ decreasing influence
- Thickness of the web: $1/t_w$ decreasing influence

II. New criteria for "strong" stiffeners

- Using most critical stiffness (GMNIA)
- Based on b_1/t_w - ratio
- Usable for (1), 2 and 3 stiffeners
- More accurate than EN 1993-1-5 criteria $\gamma_{s_opt} = b_1 * \left(\frac{3 * 10^6}{b_1^{1.968} * t_w} \right) + 135$

3. Results & Discussion

I. Influence of b_1/t_w - ratio

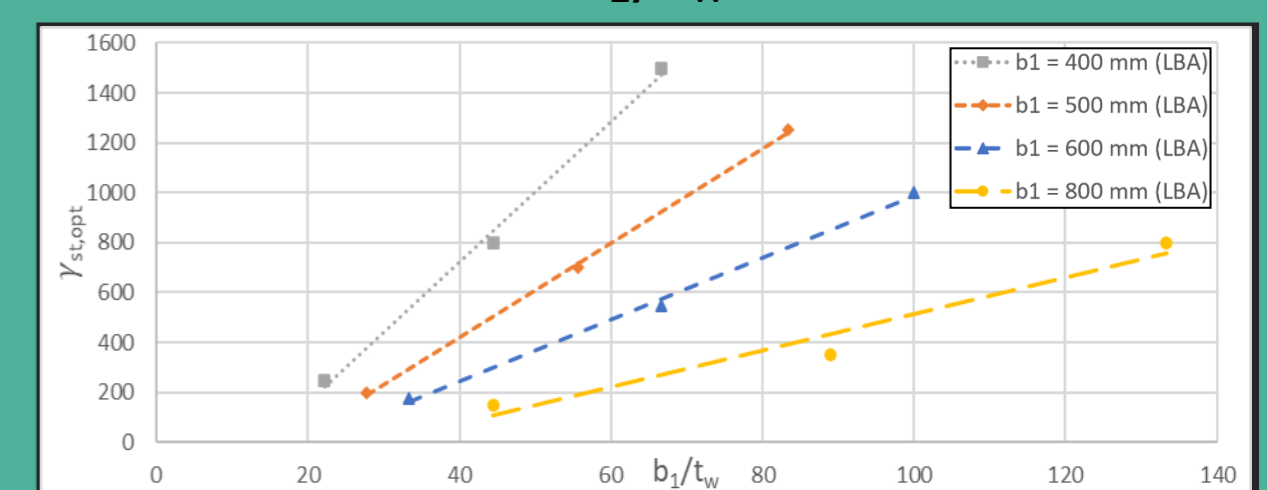


Figure 6: Optimal stiffness (LBA) in function of the ratio b_1/t_w (max values)

II. Influence of s_s , a , h_w and t_w

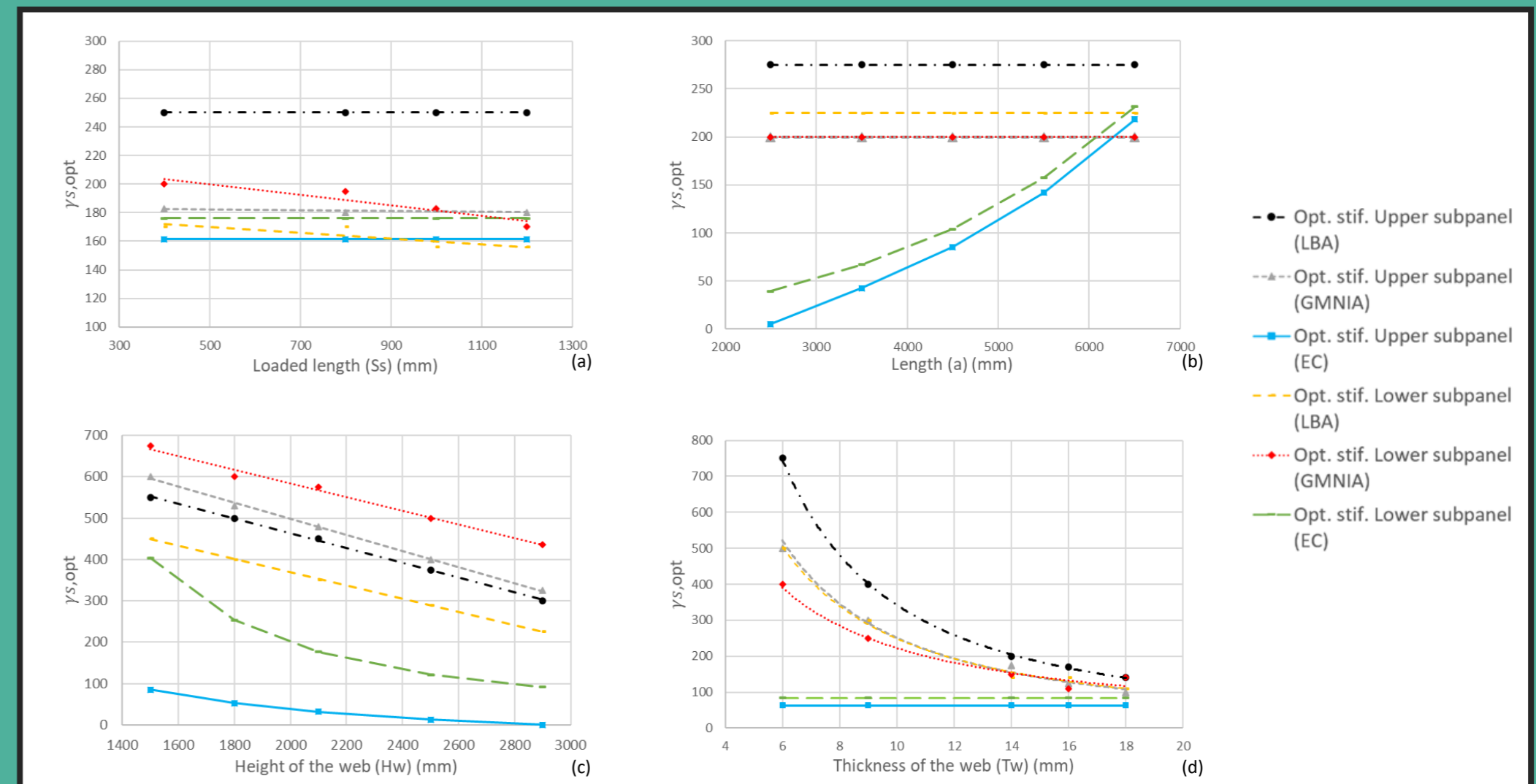


Figure 7: Effect on the optimal stiffness of different parameters according to EN 1993-1-5 and numerical results: a) loaded length, b) length, c) height of the web, d) thickness of the web

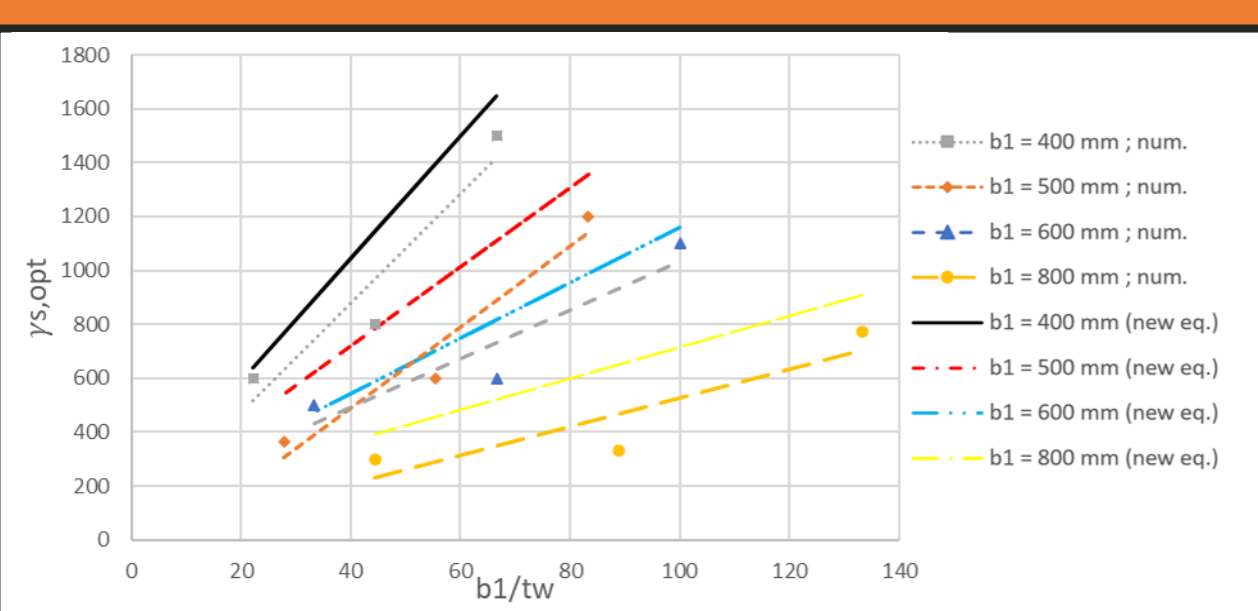


Figure 8: Optimal stiffness (GMNIA) in function of ratio b_1/t_w

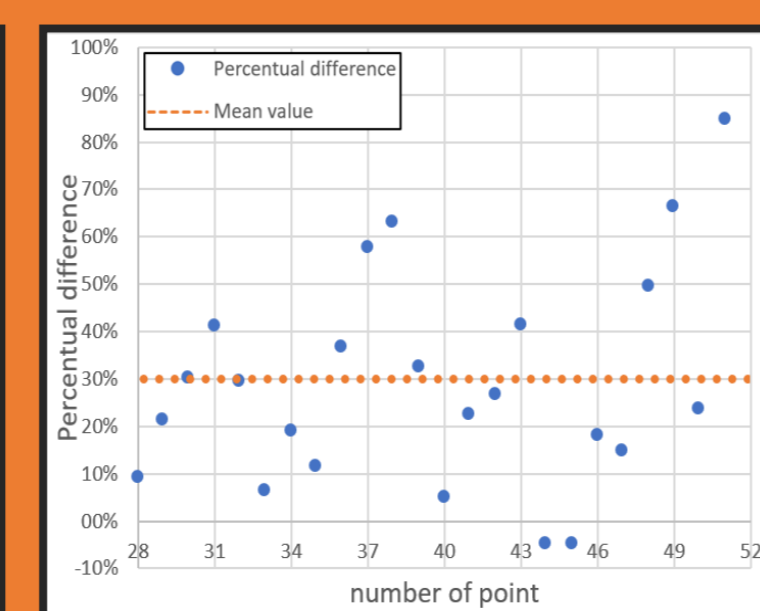


Figure 9: Percentual difference of new formulation and EN 1993-1-5

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[1] B. Kövesdi en L. Dunai, Patch loading resistance of girders with longitudinally stiffened webs (powerpoint), Munich, Germany, 2019.
[2] M. R. Hirmand, E. Rahimi, A. Moghadam en H. T. Riahi, „A mathematical investigation on the optimum design of the nose-deck system in incrementally launched bridges,” European journal of scientific research, pp. 38-52, 2013.
[3] B. Kövesdi, Patch loading resistance of slender plate girders with longitudinal stiffeners, Hungary: Budapest University of Technology and Economics.