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Tuning electricity generation throughout the year with PV module technology Peer-reviewed author version

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- Tuning electricity generation throughout the year with PV module L technology 2
- Patrizio Manganiello<sup>a,b,1</sup>, Jonathan Govaerts<sup>a,b\*</sup>, Imre T. Horvath<sup>a,b</sup>, Gofran 3 Chowdhury<sup>a,b,c</sup>, Georgi H. Yordanov<sup>b,c</sup>, Hans Goverde<sup>a,b,2</sup>, Bader Aldalali<sup>d</sup>, Ian 4 Beausoleil-Morrison<sup>e</sup>, Seppo Valkealahti<sup>f</sup>, Kari Lappalainen<sup>f</sup>, Jef Poortmans<sup>a,b,c,g</sup> 5
- 6 <sup>a</sup>imec, Kapeldreef 75, Leuven, Belgium; 7 <sup>b</sup>EnergyVille, ThorPark 8310, Genk, Belgium; 8 <sup>c</sup>University of Leuven, Dept. of Electrical Engineering (ESAT), Leuven, Belgium; 9 <sup>d</sup>Kuwait University, College of Engineering and Petroleum, Khaldiya, Kuwait; 10 e3Carleton University, Ottawa, Canada; 11 <sup>†</sup>Tampere University of Technology, Electrical Energy Engineering, Tampere, Finland; 12
  - <sup>9</sup>University of Hasselt, Martelarenlaan 42, Hasselt, Belgium.

13 \*Corresponding author, email: Jonathan.Govaerts@imec.be; 1now with TUDelft; 2now with Jan De Nul

#### Abstract 14

15 Currently, photovoltaic (PV) installations target a maximization of annual energy yield. In the future however, electricity generation may need to match better with the load 16 17 profiles in a given environment and climate. In particular this will be a challenge for 18 generation across the seasons, where electrical storage is less suitable, and in the 19 built environment, where wind turbines for generation are much more difficult to 20 integrate.

21 In this paper we discuss how this challenge may be addressed with climate- and 22 consumption-specific PV module technology. In particular, we demonstrate how the 23 temperature coefficient of a PV system can impact the energy yield throughout the 24 year. After explaining the concept, we apply our electrical-optical-thermal model to do 25 very accurate physics-based bottom-up simulations in different climates. As such, 26 depending on the climate and latitude, a higher temperature coefficient of the PV 27 module may lead to higher energy yields, mostly during the colder season. We also 28 demonstrate that, if higher temperature coefficients are accompanied by improved 29 low-light performance (tunable using the module's series resistance), the seasonal 30 gain can be much higher. We indicate the relevance of our assumptions by basing the 31 module performance in the simulations on (datasheets of) commercial modules.

#### 32 **Keywords**

33 PV module technology, energy yield simulation, temperature coefficient, low-light performance, seasonal balancing by tuning PV generation 34

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#### 1. Background 36

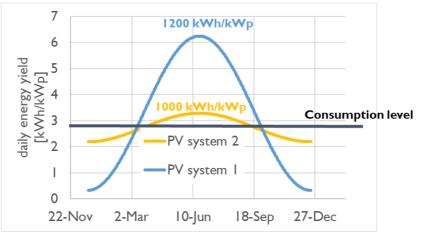
37 Currently, the main target in photovoltaic (PV) installations is on getting as much energy as possible out of a module, resulting in a maximization of annual energy yield, 38

namely the energy produced (kWh) per installed nominal power (kWp), in order toachieve the highest possible return on investment. This is a good target in case of:

- Low PV penetration rates such that PV electricity can be easily absorbed by the
   grid
- A generation profile reasonably aligned to the consumption profile (e.g. cooling
   needs in hot climates)
- 45 Expensive modules/systems
- A fixed electricity pricing throughout the year

47 In general, it is a good target if the grid overhead (distribution cost) is limited and the 48 generated energy can be immediately (and locally) consumed, or if storage is readily 49 available (and cheap). However, this is not necessarily the case if the grid overhead 50 dominates over module cost, so in the opposite situation of high PV penetration rate, 51 mismatch between generation and consumption, cheap modules/systems and low or 52 even negative electricity pricing in PV production highs. In such an environment, it 53 may be beneficial to look at better balancing generation and load profiles. This can be 54 done through demand-side-management and integration of storage in the system, but 55 also from the generation side, by tuning the production peaks towards the times of 56 need. It can be relevant on a seasonal level, as well as intraday, and one of the easiest 57 ways of doing this is by optimizing orientation and tilt angles of PV generators, but also 58 the temperature-dependent performance of the used modules can provide a knob for 59 such tuning.

- 60 In particular for colder climates, it can be of interest to reduce overall yearly energy
- 61 yield in favor of a better match in the cold season. Figure 1 conceptually, in an extreme
- 62 situation, illustrates how a PV system (PV system 2 in Figure 1) may better match the
- 63 consumption level (in this case fixed throughout the year) than a system maximizing
- 64 overall yearly energy yield (PV system 1 in Figure 1).



66 Figure 1: Conceptual illustration indicating how a PV system may sacrifice its overall

- 67 yearly energy yield for a better match to the seasonal consumption level
- 68

69 While PV systems are typically already matching consumption by default in warmer 70 climates, where production is well aligned with the demand for electrical cooling [1], in 71 colder climates yearly energy yield is sometimes sacrificed for matching daily morning 72 and evening peaks (east-west orientation) or seasonal variations (tilt). Especially the 73 latter one is of interest, since the former one can be solved relatively straightforward 74 through electrical storage, while on a seasonal level this would be much more 75 challenging and costly. Figure 2 illustrates how tilting a South-oriented panel allows to 76 influence its yearly insolation, and therefore energy generation, profile. This simulation 77 illustrates how difficult (or impossible) it is in the Paris climate to optimize for winter 78 production with varying tilt alone, while it is very easy in Kuwait, given the constant 79 amount of sunlight.

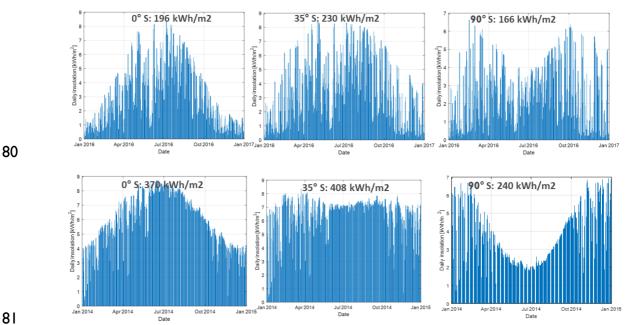


Figure 2: Impact of tilt angle (0°, 35° and 90°) on received daily insolation (across a
full year) and overall yearly energy production of a south-oriented panel for Paris
(top) and Kuwait (bottom)

85

On the other hand, the PV module technology itself is sometimes adapted to cope with
the installation climate and environment, though implementation is usually focused on
limiting degradation (e.g. extra moisture intrusion protection in hot-humid conditions
or radiation protection in high UV conditions or space) and overall performance losses
(e.g. increased metal cross-sections for cell interconnection for systems with higher
peak irradiance of the modules due to climatic conditions or bifaciality).

92 The above approaches mainly focus on the first-order effects induced by variations in 93 irradiation. In this paper, we want to indicate another possibility to take into account 94 the expected climate and consumption patterns for a system, in particular the second-95 order effects of temperature on the performance, by tuning the temperature coefficient 96 (TC) for maximum power of the PV module technology to be used. Figure 3 shows 97 conceptually and greatly simplified, how the cell temperature will result in a flattening
98 of the energy yield output over the year, and increasingly so for modules with a higher
99 temperature coefficient. Depending on the exact conditions, the energy yield could
100 even be potentially higher in the cold season for modules with a higher temperature
101 coefficient.

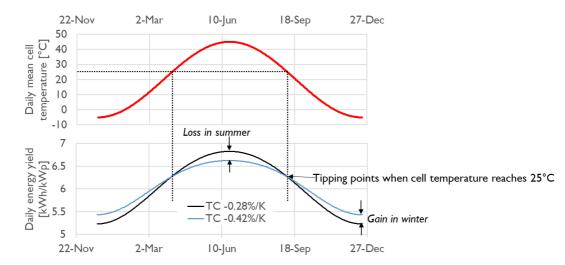


Figure 3: Conceptual indication of the impact of differences in temperature coefficient
 for maximum power (TC) on seasonal energy yield fluctuations

105

102

# 106 2. Modeling framework, climate data and module 107 assumptions

108 To check the real impact of realistic TCs on energy yield in actual conditions 109 throughout the year, we apply our advanced modeling framework [2]-[2] to four 110 hypothetical PV installations at different latitudes experiencing varying climatic 111 conditions and with varying PV module technology. Figure 4 shows the buildup of the 112 used modeling framework. As the framework is only applied here, we refer to [2] and 113 [2] for more information including detailed explanations and validation experiments.

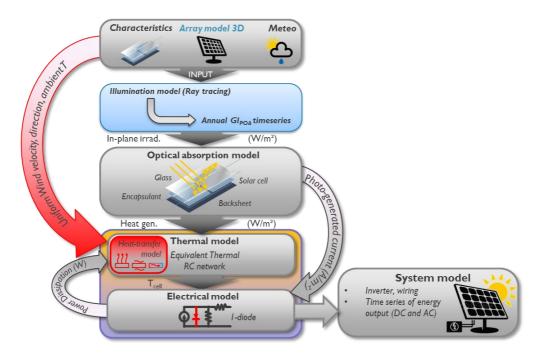


Figure 4: Conceptual representation of the used modeling framework [2], [2]

117

Climate data have been collected across a full year with a resolution of 1 minute from 118 4 locations: Kuwait City (Kuwait), Oldenburg (Germany), Ottawa (Canada) and 119 120 Tampere (Finland). These diverse locations allow to illustrate the impact of the 121 temperature coefficient of the module technology in different climates and latitudes. 122 Measured wind velocity (speed and direction), ambient temperature, Global Horizontal Irradiance (GHI) and Diffuse Horizontal Irradiance (DHI) were available at every 123 location. Using the Perez model [3], [5], Plane-Of-Array (POA) Irradiance is calculated 124 125 (from the GHI and DHI values) at every location for the full year. We assume the PV 126 panels are South-oriented, with tilt angle at each latitude optimized for annual energy yield [6], as shown in Table 1, where also their respective Köppen-Geiger classification 127 [7] is displayed. 128

- 129
- 130 131

Table 1. Tilt angles [6] and climate classifications [7] for the PV installations simulated in the study

Location	Tilt angle [°]	Köppen-Geiger climate classification
Kuwait City (Kuwait)	26	BWh
Oldenburg (Germany)	33	Cfb
Ottawa (Canada)	37	Dfb
Tampere (Finland)	40	Dfb

I33 Stand-alone commercially available conventional PV modules made of 60 cells inI34 portrait installation have been considered for the energy yield simulations. Hence,

135 module-level maximum power point tracking (MPPT) has been assumed. For the

136 temperature-dependent PV module behaviour, we always refer to the temperature

137 coefficient for maximum power abbreviated as TC.

138

# **3. Energy yield simulations: results and discussion**

140 The simulations have been carried out to determine absolute and relative differences 141 in energy yield between PV module technology that is currently commercially 142 available. As such, the module parameters needed for these simulations, namely 143 photo-generated current, temperature-independent coefficient of diode saturation 144 current, diode ideality factor, and series and shunt resistances, have been calibrated 145 directly from actual module datasheets. Each time, modules with same rated power 146 and area have been selected to ease comparison.

147

# 148 3.1 Impact of temperature coefficient

149 In this first case, two different types of PV module have been considered, one with a 150 temperature coefficient for maximum power (TC) equal to -0.42 %/°C [8], the other 151 with a temperature coefficient for maximum power equal to -0.28 %/°C [9]. In the 152 following, we refer to them as HTC and LTC, respectively. These modules have been 153 chosen as their TC values are representative of the extremes currently available in the high-end market. Based on the datasheet values, summarized in Table 2, the HTC 154 155 module could be representative for state-of-the-art PERC technology, while the higher Voc for the LTC module indicates a technology with passivated contacts. 156

- 157
- 158

Table 2. PV module parameters from datasheets

Parameter	HTC [8]	<i>LTC</i> [9]
Short-circuit current <i>I</i> <sub>sc</sub> [A]	9.78	9.38
Open-circuit voltage Voc [V]	40.26	43.89
Maximum power <i>P<sub>mp</sub></i> [W]	305	305
Current at maximum power Imp [W]	9.31	8.66
Voltage at maximum power V <sub>mp</sub> [W]	32.76	35.22
Temperature coefficient of <i>P<sub>mp</sub></i> (TC) [%/ <sup>o</sup> C]	-0.42	-0.28

160 For detailed (daily) accurate energy yield simulations is important to also assess the low-light performance of both modules as much as possible from the information 161 available in the respective datasheets. In the case of LTC [9], it is claimed that the PV 162 163 module shows "3.5% relative efficiency reduction at low irradiance (200 W/m<sup>2</sup>)", 164 whereas the datasheet of HTC [8] includes a graphic of normalized peak power as a function of irradiance. This information has been included in the module parameters' 165 fitting procedure, leading to the results shown in Figure 5. From Figure 5(a), it is 166 evident that LTC performs better than HTC at low light. On the other hand, Figure 5(b) 167 168 shows that LTC performs worse than HTC when the temperature is below 25 °C. Thus, the improved efficiency of HTC due to lower temperature in cold climates is 169 170 counteracted by a decreased efficiency at low irradiation. In the following subsections, we elaborate and discuss the relative outcome of the simulations with the two PV 171 172 modules in the cases of the four installation sites using their relevant climatic data.

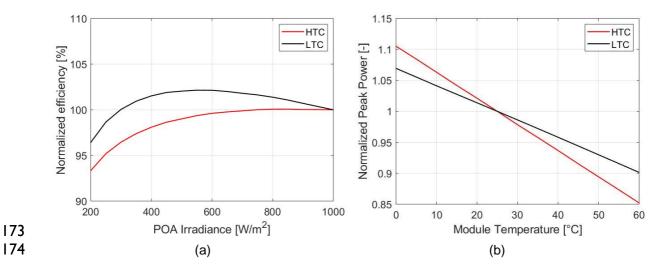
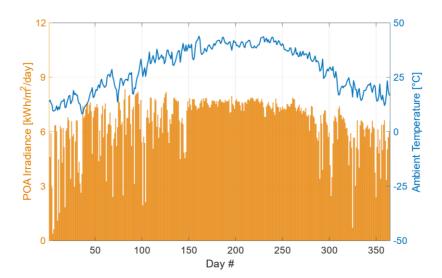


Figure 5: Performance of the PV modules under analysis. (a) low-light behavior at a fixed cell temperature of 25 °C and (b) Thermal behavior at a fixed irradiation of 1000 W/m<sup>2</sup>.

#### 178 **3.1.1 Kuwait installation**

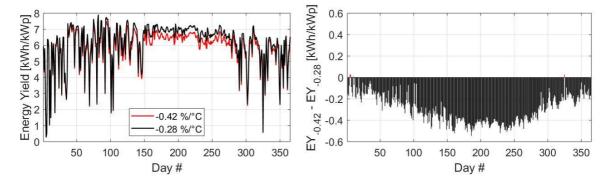
Starting with the hottest climate, at a latitude of 29.4°N, it is immediately clear that
here a low temperature coefficient is highly preferable. With an average ambient
temperature of 29°C and high irradiation levels throughout the year, as shown in
Figure 6, the cell temperatures are obviously continuously over 25°C (with an average
over operational hours higher than 40°C).



184

Figure 6: Daily POA irradiance (orange bars) and daily average (over operational hours) ambient temperature (blue curve) values throughout 2014, obtained from the *Kuwait data used for the simulations.*

Figure 7 shows the simulated daily energy yields as well as the difference between the two PV modules. As the energy yield is referenced to the nominal power (Wp) of the module at 25°C, the high operational temperature will lead to improved energy yields for PV modules with a lower temperature coefficient. As expected, with the exception of a few days, PV modules with a lower temperature coefficient generate a higher energy yield all over the year in this type of climate.



195

Figure 7: simulated daily energy yield throughout 2014 for the HTC and LTC
modules (left), and the resulting difference (right). Red bars in the right plot refer to
days where the HTC module leads to a higher energy yield (positive values in the
graph, almost none present) than the LTC module. The opposite case is represented
by the black negative bars.

201

While the relative annual energy yield difference amounts to -4.8%, cf. Table 3, the
difference peaks to -6.4% in the summer season, as shown further on in Figure 15.
Moreover, hot desert climates as in Kuwait require little heating in winter, but all the
more cooling in summer. This translates in an increased electricity consumption in

summer [1], and so the higher production from the low-temperature-coefficient PVsystem is even more attractive.

208

### 209 3.1.2 Oldenburg installation

210 In a more moderate climate in Western Europe, at a latitude of 53.1°N, the results are 211 somewhat similar to the Kuwait ones, but with many additional days of gain due to the 212 use of PV modules with a higher thermal coefficient. With the lower overall 213 temperature and higher fluctuations in irradiance, shown in Figure 8, the differences 214 in daily energy yield between different PV module temperature coefficients for the simulated year are smaller than in Kuwait. As shown in Figure 9, the use of PV 215 216 modules with a higher thermal coefficient allows for a slightly higher overall energy 217 yield during the first and last months of the year, thus during fall and winter months. 218 However, the losses during spring and summer are much higher, leading at last to a 219 yearly energy loss around 2.4% (Table 3).

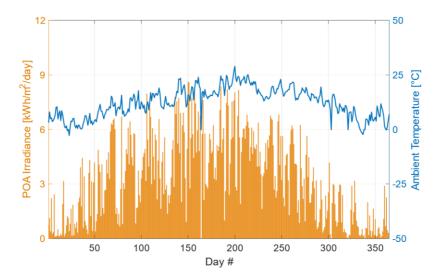


Figure 8: Daily POA irradiance (orange bars) and daily average (over operational
 hours) ambient temperature (blue curve) values throughout 2014, obtained from the
 Oldenburg data used for the simulations.

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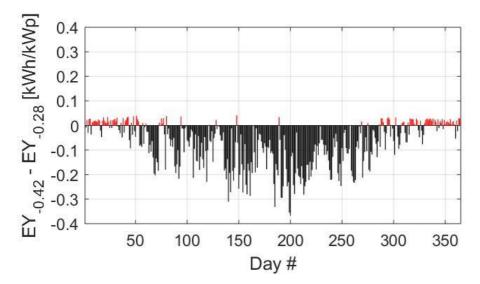


Figure 9: Simulated daily energy yield differences throughout 2014 for Oldenburg.
Red bars in the right plot refer to days where the HTC module leads to a higher
energy yield (positive values in the graph) than the LTC module. The opposite case
is represented by the black negative bars.

225

#### 23 3.1.3 Ottawa installation

At a slightly more southern latitude of 45.4°N, Ottawa boasts a higher yearly insolation than Oldenburg, but at the same time experiences more extreme temperature variations typical of an inland climate, and a lower mean ambient temperature of 8.8°C during operational hours, as is illustrated in Figure 10. This results in a significantly better performance of PV modules with higher thermal coefficients during winter months and comparable performance of HTC and LTC modules during fall months, as shown in Figure 11 and Figure 14.

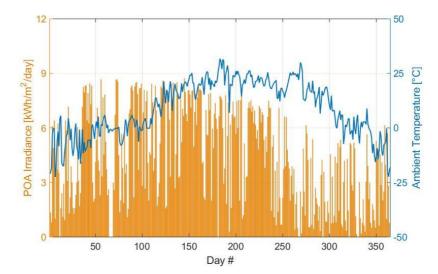


Figure 10: Daily POA insolation (orange bars) and daily average (over operational hours) ambient temperature (blue curve) values throughout 2018, obtained from the Ottawa data used for the simulations.

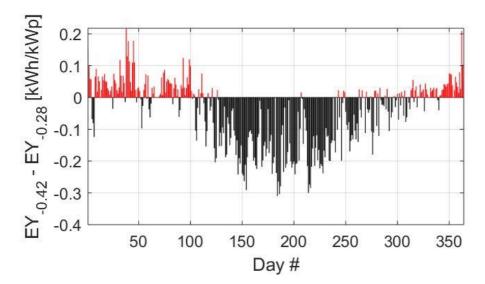


Figure 11: Simulated daily energy yield differences throughout 2018 for Ottawa. Red
bars in the right plot refer to days where the HTC module leads to a higher energy
yield (positive values in the graph) than the LTC module. The opposite case is
represented by the black negative bars.

248

The use of PV modules with a higher thermal coefficient in this type of climate leads to limited yearly energy yield losses of about 1%. In this location however, heating and electricity consumption are much higher in winter, so the relevance of producing more in winter could favor PV modules with a higher temperature coefficient.

253

#### 254 **3.1.4 Tampere installation**

Much more North, at a latitude of 61.5°N, and as shown in Figure 12, Tampere irradiation is somewhat lower than Oldenburg, especially noticeable in winter. Such low irradiation during winter is partly due to the weather station setup, that is described in detail in [10], where the pyranometer suffers from some shading due to building structures in the morning (all year) and in the evening (in winter), as well as snow/ice coverage in winter.

On the other hand, average ambient temperature over operating hours is deeply below 261 262 25°C, with a yearly average of 6.5°C. As shown in Figure 13, in this climate the 263 advantages of a higher temperature coefficient are similar to the Ottawa case, though 264 with more limited gain. As shown in Figure 15, slightly better performance of PV 265 modules with higher thermal coefficients are obtained during winter months whereas 266 slightly worse performance occurs during fall months. As for Ottawa, in Tampere 267 heating and electricity consumption are much higher in colder seasons, so the 268 relevance of producing relatively more during winter could favor PV modules with a 269 higher temperature coefficient. The use of PV modules with a higher temperature 270 coefficient in this type of climate leads to yearly energy yield losses slightly above 1%.

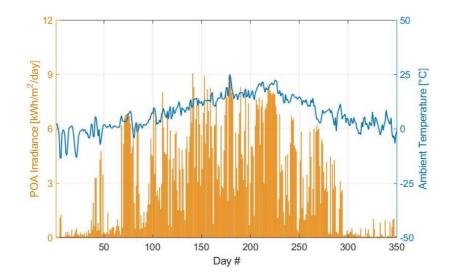
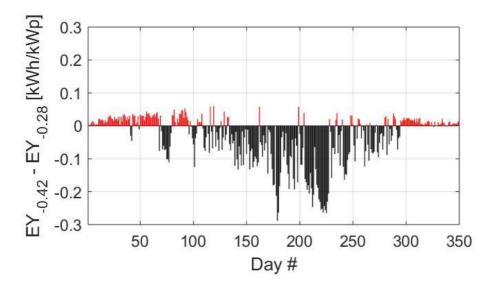


Figure 12: Daily POA insolation (orange bars) and daily average (over operational hours) ambient temperature (blue curve) values throughout 2015, obtained from the Tampere data used for the simulations.



276

Figure 13: Simulated daily energy yield differences throughout 2015 for Tampere.
Red bars in the right plot refer to days where the HTC module leads to a higher
energy yield (positive values in the graph) than the LTC module. The opposite case
is represented by the black negative bars.

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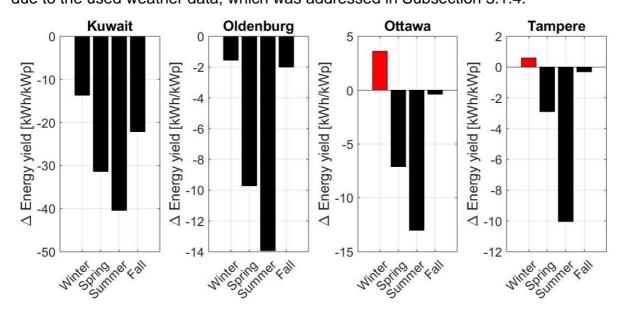
## 282 3.1.5 Overview of the simulated installations

Table 3 recapitulates the results, indicating the impact of temperature coefficient of
the PV modules on energy yield, depending on the climate, and based on actual
weather data. Though these numbers only give the annual differences, the impact can
be much higher at particular moments and locations.

		Kuwait	Oldenburg	Ottawa	Tampere
Yearly POA irradiance [kWh/m <sup>2</sup> ]		2381	1196	1597	1121
Daily variation [kWh/m <sup>2</sup> ]		1.46	2.32	2.69	2.74
Mean daytime ambient temperature* [ºC]		28.9	12.3	8.8	6.5
Annual energy yield [kWh/kWp]	HTC	2130	1126	1560	1025
	LTC	2238	1153	1577	1038
Gain with higher TC [%]	Annual	-4.8	-2.4	–1.1	-1.2

288 Table 3: overview of yearly weather data and simulated energy yields for all locations

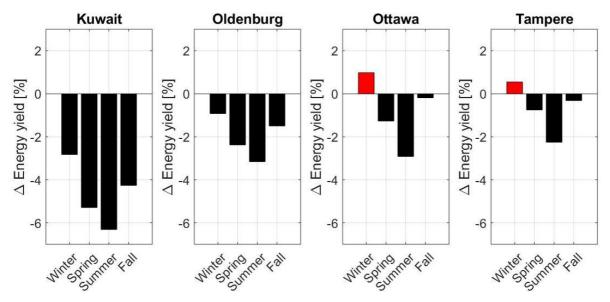
The benefits related to higher thermal coefficients in colder climates are more visible if the energy yield gain is split per season, as in Figure 14. In colder climates as Ottawa and Tampere, energy production during warmer seasons is sacrificed to allow energy yield gain during winter. As a consequence, a better production-demand matching may be obtained. It is worth to note that Tampere's potential is not fully acknowledged due to the used weather data, which was addressed in Subsection 3.1.4.



296

297 Figure 14: Seasonal absolute gain due to a higher thermal coefficient of the PV
298 module for the different locations. Red bars in the right plot refer to days where the
299 HTC module leads to a higher energy yield (positive values in the graph) than the
300 LTC module. The opposite case is represented by the black negative bars.

302 Considering also the absolute energy yield values for the seasons, Figure 15 shows 303 the same graph in terms of relative gains. While losses can be very significant for a 304 Kuwait climate, amounting to almost 7%, 1% additional energy during winter may 305 become interesting for colder climates as Ottawa and Tampere. It is important to note 306 though that the effects of snow accumulation on the PV modules was not considered 307 in the simulations.



308

Figure 15: Seasonal relative gain due to higher thermal coefficient for the different
locations. Red bars refer to seasons where the HTC module leads to higher energy
yield (positive values in the graph) than the LTC module. The opposite case is
represented by black negative bars.

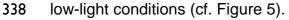
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# 314 3.2 Impact of (improved) low light behaviour

315 In this Section, we will demonstrate that the energy yield of PV modules with higher thermal coefficients in cold climates can be significantly improved if such a higher 316 317 thermal coefficient is combined with an improved low light performance. To clarify this 318 point, we will start with the analysis of the typical operating conditions of the HTC 319 module under Kuwait and Ottawa climates in terms of irradiation and PV module 320 temperature, summarized in Figure 16 and Table 4. Specifically, Figure 16 shows the 321 occurrences of a given set of operating conditions. Given the minute resolution of the 322 climate datasets, colors in Figure 16 show for how many minutes the PV module was 323 subjected to a certain irradiance (x-axis) and working at a certain module temperature 324 (y-axis). In Table 4, the same results are summarized for given ranges of PV module 325 temperature and irradiation.

From Figure 16, it is evident that, as expected, production under Kuwait climate occurs
 most of the time at medium to high module temperatures, and mainly under two
 different operating conditions: high irradiation around 1000 W/m<sup>2</sup> with high module
 temperature in the range 50-60 °C, and low irradiation below 200 W/m<sup>2</sup> with "medium"

330 module temperature in the range 22-32 °C. On the other hand, Ottawa climate shows clear peaks at low irradiation around 200 W/m<sup>2</sup> and low module temperature in the 331 range 14-24 °C as well as at 0 °C. Also, energy production below 25 °C is dominant in 332 333 such a climate, as shown in Table 4. Purely looking at temperature coefficients, in a 334 climate like Ottawa much better performance of the HTC module is expected than 335 what is shown in the Section 3.1.3. This expectation is skewed because performance at low temperature often happens in low light conditions, such that improvements due 336 337 to the higher temperature coefficient are counteracted by lower module efficiency at



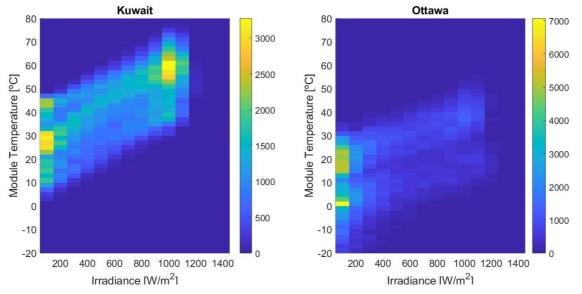


Figure 16: Occurrences (in minutes) of different operating conditions for HTC PV
module. Colors show how many minutes the PV module was subjected to a certain
irradiance (x-axis) and working at a certain module temperature (y-axis) during one
year.

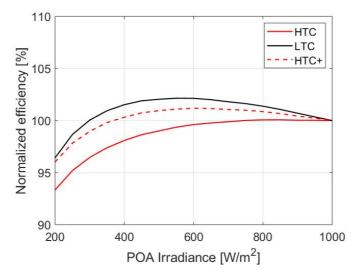
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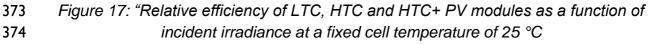
Table 4: Occurrences (in percentages of daytime hours in a full year) of different
operating conditions, in terms of irradiance and PV module temperature ranges, for a
HTC PV module in the Ottawa climate

Irradiance [W/m <sup>2</sup> ]	0-200	200-800	800-1500	Total by row
Module Temper. [°C]				
-45 - +25	41.6	22.7	6.2	70.5
+25 - +85	4.4	13.5	11.7	29.5
Total by column	46.0	36.2	17.8	

349 However, performance at low irradiation can be engineered by proper cell and module 350 design. As shown in [10], shunt and series resistances strongly affect low light 351 performance of PV modules. Of particular interest is the effect of series resistance for tuning the low light behavior: the higher it is, the better the relative efficiency in the 352 mid-irradiation range. With high series resistance, relative efficiencies higher than 353 354 100% can be obtained in the range 300 to 1000 W/m<sup>2</sup>. This is the case for the LTC 355 module shown in Figure 5. Therefore, although counter-intuitive, a higher series 356 resistance could be beneficial for modules with higher thermal coefficients in cold 357 climates at high latitude. Again, the starting point has been a real 305 Wp PV module [12] with the same temperature coefficient for maximum power as the HTC module, 358 359 namely -0.42 %/°C. Parameter fitting has been performed for such a module as discussed before. Since the datasheet does not provide any usable information about 360 361 the low light performance, the parameter fitting has been done only considering 362 performance at STC and temperature coefficients. Figure 17 shows the results in 363 terms of low-light performance at 25°C in comparison with the low temperature coefficient LTC module. It is clear that behavior in low-light is very similar for the two 364 PV modules, although the performance of the LTC module is still better. Compared to 365 Figure 5, low-light performance of this new high temperature coefficient PV module, 366 367 referred to as HTC+, is much better than the one of HTC. It is worth to note that the 368 fitted series resistance of HTC+ is indeed higher than the fitted series resistance of 369 HTC. This is consistent with the lower Fill Factor, 0.755 and 0.775, respectively, and 370 the lower number of busbars, 3 and 4, respectively, of HTC+ compared to HTC, as 371 from their datasheets.







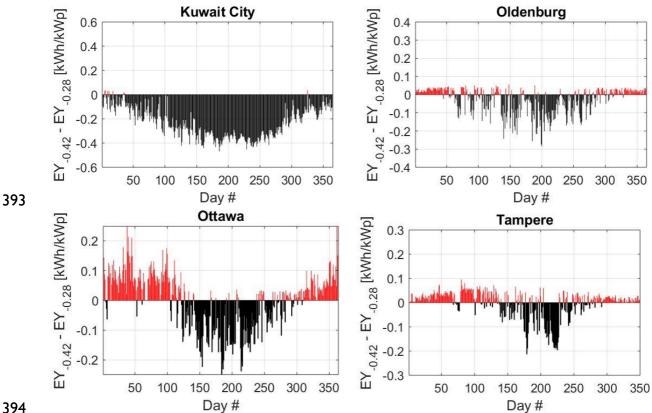
The joint effects of higher temperature coefficient and improved low-light performance have been simulated with the new HTC+ PV module model again for the same 4 locations. Results are summarized in Table 5, Figure 18 and Figure 19. Table 5 recapitulates the results, indicating the impact of temperature coefficient of the PV 379 modules on energy yield, depending on the climate, based on actual weather data. As 380 for the results presented in Table 3, these numbers only give the annual differences. 381 However, the impact can be much higher at particular moments and locations. The 382 benefits related to higher thermal coefficients in colder climates are more visible if the 383 energy yield gain is split per season, as in Figure 18 and Figure 19. In colder climates, 384 energy production during summer is sacrificed to allow energy yield gain during colder seasons. As a consequence, a better production-demand matching may be obtained. 385 386 Particularly interesting are locations such as Ottawa and Tampere where, together 387 with a better spread of production along the whole year, negligible yearlong losses are introduced if PV modules with a lower temperature coefficient are replaced with PV 388 389 modules with a higher one and a properly engineered low-light behaviour.

390

Table 5: overview of simulated yearly energy yields of HTC+ and LTC PV modules 391 for all locations

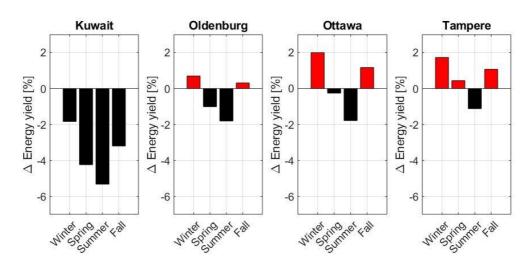
		Kuwait	Oldenburg	Ottawa	Tampere
Annual energy yield [kWh/kWp]	HTC+	2153	1142	1578	1038
	LTC	2238	1153	1577	1038
Gain for HTC+ modules [%]	Annual	-3.8	-0.9	-0.1	+0.0

392



395 Figure 18: Simulated daily energy yield differences between HTC+ and LTC PV 396 modules for the different climates as in Figures 7, 9, 11 and 13.

397



398

399 Figure 19: Seasonal relative energy yield gains of HTC+ PV modules with respect to 400 LTC modules for the different locations. Red bars refer to seasons where the HTC+ 401 module leads to a higher energy yield (positive values in the graph) than the LTC 402 module. The opposite case is represented by black negative bars.

403

404 Both Oldenburg and Ottawa show energy gains with the HTC+ module during winter 405 and fall. However, in Tampere the advantages of a higher temperature coefficient are 406 visible almost all over the year, with additional energy generated during three seasons 407 out of four. It is only during summer that the PV modules with lower temperature coefficients are performing better, as evident from Figure 18. Additionally, if snow 408 409 cleaning is duly implemented during winter and shading is avoided, in a climate as 410 Tampere there might even be an overall increase in the yearly energy yield.

411

#### 4. Conclusion 412

413 In this paper, we point out the impact of the temperature coefficient of PV modules on energy yield throughout the year, indicating also the somewhat counterintuitive 414 415 benefits that a high temperature coefficient may have depending on the climate where 416 it is operational. If low-light behavior is not optimized and only a higher temperature 417 coefficient is considered, some seasonal gain is obtained in 2 out of 4 locations, namely Tampere and Ottawa, whereas in Oldenburg's and Kuwait's climate PV 418 419 modules with a lower temperature coefficient would lead to better performance. 420 However, when a higher temperature coefficient is accompanied by improved low-light 421 performance, the benefits of such PV modules become clear. Except for the Kuwait 422 case, higher production during cold seasons, beneficial for a better production-423 demand matching, is obtained in all the other cases. For the specific case of Tampere, 424 the use of such PV modules could even lead to an overall increase of the yearly energy

425 yield. Considering little attention is currently paid to times of low PV production, we426 also point out the potential impact of shading objects or snow cover that may affect427 results.

428

## 429 **Context and outlook**

The findings here are meant to fit into a bigger picture in the future where PV 430 43 I production will be optimized to times of electricity scarcity rather than maximizing annual energy yield. Such optimization should then also include "suboptimal" tilt 432 433 angles combined with the effects reported here. Furthermore, the potential gains and 434 losses here are only expressed as a function of produced electrical energy, as most 435 scientific and technical approach, but market-driven dynamic pricing will further alter 436 the outcome and will obviously need to be assessed in any future practical 437 implementation.

438

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