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Early structural build-up behavior, setting mechanism, and nanostructure of alkali-activated GGBFS mixtures Peer-reviewed author version

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18	Abstract								
20	The initial changes in the microstructure of Alkali-activated slag cement (AAS) characterize the								
21	rheological behavior, initial structuration and setting times of the mixture. In this study, the								
22	relationships between the rheological behavior, solidification process and nanostructure changes of								
23	sodium hydroxide-activated slag (NH-AAS) and sodium silicate-activated slag (SS-AAS) pastes over								
24	time are investigated by small amplitude oscillation test, isothermal calorimetry, SEM analyses and								
25	¹ H- ²⁹ Si cross-polarization magic angle spinning nuclear magnetic resonance spectroscopy (CP MAS								
26	NMR) and ²⁹ Si MAS NMR spectroscopy. Test results showed that the NH-AAS reaches its initial								
27	setting time following a continuously proceeding structuration process, while the SS-AAS reaches its								
28	initial setting with an abrupt increase in the structuration process. At their initial setting times, the NH-								
29	AAS and SS-AAS mixtures release similar heat and reach a similar reaction degree. The SS-AAS								
30	mixture had more N-A-S-H formation than C-A-S-H at the initial setting time. On the other hand, the								
31	amount of C-A-S-H was similar to N-A-S-H in the NH-AAS mixture. The gradual N-A-S-H gel								

32 degradation to form C-A-S-H was observed during the acceleration period for the SS-AAS mixture.

- *Keywords*: Structural build-up, Setting time, Nanostructure, Nuclear magnetic resonance
- 35 spectroscopy (NMR), Alkali-activated cements, Ground granulated blast furnace slag.

37 1. Introduction

38 Alkali-activated cement (AAC) has been considered as a low carbon footprint alternative to Portland 39 cement (PC) due to its higher mechanical properties, better volume stability, and greater resistance to 40 sulfate and acid attack depending on the precursor type [1]. Alkali-activated slag cement (AAS) is a 41 common and promising type of AAC, as their production uses ground granulated blast furnace slag 42 (GGBFS), an industrial by-product, and substantially reduces the CO₂ emission [2], [3]. However, although numerous studies have explored the mechanical properties and durability of AAS [2]-[5], 43 44 very few studies have focused on their microstructural changes over time influencing the rheological 45 properties and setting behavior [6], [7].

46

47 The rise in structural build-up of cementitious materials results from the combination of physical 48 interactions and chemical hydration [7], [8]. In Portland cement, the setting process can roughly be 49 divided into three stages: (i) a colloidal percolation network is formed due to colloidal interactions 50 between cement particles, (ii) cement particles are rigidly connected by the early reaction products 51 such as nano-size C-S-H bridges, (iii) C-S-H bridges are further strengthened, leading to a percolated 52 rigid network [9]. Recently, a few authors have also explained the increase in the early structural 53 build-up of AAC. Alnahhal et al. [10] compared the viscoelastic behavior between alkali-activated 54 slag/fly ash and cement pastes and found that the colloidal attraction between cement particles was 55 significantly stronger than the cohesiveness of the very early inter-particle gel contacts generated in 56 alkali-activated slag/fly ash pastes. They stated that the accumulation of initial reaction products was a 57 possible reason for reaching the solid-like state in the sodium silicate-activated mixtures. In contrast, 58 reaching the solid-like state resulted from a well-percolated network formation in cement paste. 59 Furthermore, another study [8] also pointed out that sodium hydroxide-activated mixtures could also 60 present a percolation network in the early times, a similar setting process with cement pastes. Kashani et al. [11] also investigated the relationship between surface chemistry and rheology in AAS pastes. 61 62 The authors found that the yield stress was dependent on the changes in the surface chemistry by the 63 amount of activation solutions. For example, a small addition of sodium silicate increased the zeta

potential, showing the increase in double-layer repulsive forces reducing the yield stress of AAS
pastes. On the other hand, a further increase in sodium silicate amount increased the yield stress,
possibly due to the increase in pH causing more slag dissolution resulting in the formation of reaction
products.

68

The understanding of the change in the nanostructure of AAS from mixing to initial setting time is also crucial. Palacios et al. [12] reported that the rapid loss of fluidity and fast setting of sodium silicate-activated mixtures is due to the initial precipitation of ill-defined N-A-S-H and C-N-A-S-H products. Li et al. [13] used various combined activators to understand the setting and hardening control of AAS. They elucidated that Ca (and hence also Mg) acts as a network modifier in slag glass, causing these precursors to dissolve more quickly. Fly ash, on the other hand, does not exhibit the same level of reactivity due to its chemical stability.

76

77 Acquiring knowledge of the nanostructure of AAS will also enable the industry to develop new 78 strategies to design AAS mixtures and promote their applications. The nanostructure characterization 79 of AAS can be done in different ways. For example, Chen et al. [14] used Fourier-transform infrared spectroscopy (FTIR) and observed that the Q² band shifted to larger wavenumbers and became 80 81 broader with an increase of silicate modulus in the activator solution. Puertas et al. [15] used various 82 techniques, such as X-ray diffraction (XRD), FTIR and nuclear magnetic resonance (NMR), to 83 determine the structure and composition of the main reaction products. Ismail et al. [16] used 84 environmental scanning electron microscopy (ESEM) with energy dispersive X-ray (EDX) to 85 determine the gel composition. They reported that the silicate-activated slag showed a nanostructure 86 dominated by a C-A-S-H type gel. In contrast, silicate-activated fly ash was dominated by N-A-S-H 87 'geopolymer' gel formations. However, all of the abovementioned studies have focused on the later 88 ages of AAC and cannot provide enough information about the microstructural changes at very early 89 ages.

90 Therefore, this study aims to determine the early gel composition of AAS at the initial setting time and91 investigates the relationship between the early structural build-up and nanostructure of AAS. The

92 structural build-up of AAS has been evaluated by small amplitude oscillation sweep (SAOS) tests. The 93 nanostructure of AAS was determined by the combined use of ¹H-²⁹Si cross-polarization magic-angle 94 spinning NMR (CPMAS NMR) and ²⁹Si MAS NMR. The rheological behavior and gel composition of 95 sodium hydroxide-activated (NH-AAS) and sodium silicate-activated slag mixtures (SS-AAS) at the 96 initial setting time was compared.

97

98 2. Materials and Methods

99 2.1 Materials and mix design

100 In this investigation, ground granulated blast furnace slag (GGBFS) was employed as precursor. This 101 material was provided by ORCEM, the Netherlands. Table 1 displays the results of the chemical 102 composition analyzed by X-ray fluorescence (XRF). The X-ray diffraction pattern and particle size 103 distribution of GGBFS are displayed in Fig. 1. A broad diffraction hump between 20° and 35° 20 is 104 observed due to the presence of the amorphous components and the absence of crystalline phases. 105 GGBFS has a volume-mean particle sizes (d_{50}) of around 9 µm. Sodium hydroxide pellets (NaOH, 106 caustic soda) with 97 % purity and liquid sodium silicate solution were used as activating agents. The 107 liquid sodium silicate solution consists of 28.5% SiO₂, 17.95% Na₂O and 53.55% water with an Ms 108 value (SiO₂/Na₂O) of 1.6. Sodium hydroxide was used to adjust the Ms value of the activator solution 109 to 1.2. The mixture compositions are given in Table 2. Two AAS mixtures were produced in this study; 110 the mixtures coded as NH-AAS was activated by NaOH, while the mixtures coded as SS-AAS was 111 activated by the combination of NaOH and liquid sodium silicate with a Ms value of 1.2. The water-112 to-solid binder ratio (w/sb) and sodium content (Na2O%) of the mixtures NH-AAS and SS-AAS were 113 0.45 and 5%, respectively. The pH values of activator solutions (Table 2) were determined by a pH meter at 20 °C. However, it should be noted that using a pH meter to measure the pH of the activator 114 115 solutions may result in some errors owing to the extremely high alkali ion concentrations and the 116 presence of silica in the activator solution [17].

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- 118

Precursor CaO Al_2O_3 MgO \overline{SO}_3 TiO₂ K₂O Na₂O Fe₂O₃ MnO Others SiO₂ GGBFS 40.8 7.84 0.67 0.39 0.31 33.3 12.3 2.30 1.29 0.44 0.36 121 100 (b) 6 Cumulative passing percentage (%) (a) 80 Slag 60 -Erequency (%) 3 40 -20 0 0 20 10 30 40 50 60 70 0.1 10 100 1000 0.01 10000 122 2 Theta (degrees) Particle diameter (µm) 123 Fig. 1. X-ray diffraction pattern (a) and Particle size distribution (b) of GGBFS. 124 125 Table 2. Mixture design of AAS. W/SB Mixture Ms Na₂O (%) SiO₂ (%) pН Initial Activator notation nature ratio ratio setting time (min) NH-AAS 0 5 0 Sodium 0.45 13.82 120 hydroxide SS-AAS Sodium 0.45 1.2 5 6 13.50 45 hydroxide and sodium silicate

120 Table 1. Chemical composition of the GGBFS.

126

127 *2.2 Sample preparation*

128 The activator solutions were prepared one day before usage to ensure the complete dissolution of

129 NaOH. To prepare the paste samples for rheological tests and microstructural analysis, the GGBFS

and the activator solution were mixed in a plastic container using a mechanical stirrer for 30 s at 200rpm followed by 3 min at 1800 rpm.

132

133 2.3 Experimental methods

134 2.3.1 Structural build-up and setting times of AAS pastes

135 Small amplitude oscillation shear (SAOS) tests were carried out in an oscillatory rheometer (Anton

136 Paar MCR 102) to assess the structural build-up of AAS pastes. Storage modulus measurements were

used as an indicator of the elastic portion of the mixtures. All the tests in this study were carried out ata temperature of 20 °C.

139 The testing geometry was a six-blade vane in a steel cylindrical cup, which was used to eliminate the 140 effect of slippage between the paste and the plate or the cylindrical cup during measurements [7], [18]. 141 A plastic cover was placed on the top of the cup to prevent evaporation. Prior to time-sweep tests, the 142 linear viscoelastic region (LVER) was determined by the strain-sweep test, which was a test that the 143 strain amplitude was increased from 0.0001% to 20% with a constant frequency of 1 Hz. The strain-144 sweep test results are presented in Fig. 2. The strain amplitude of 0.005% was chosen in time-sweep 145 tests to ensure two mixtures were tested in LVER [6], [7], [19], [20]. The AAS paste was then subjected to pre-shear at 100 s⁻¹ for 30 s and rest for another 30 s to eliminate the residual stress. The 146 147 SAOS time-sweep tests were immediately started at the age of 6 min.

148



149



Fig. 2. Strain-sweep of AAS pastes for the determination of the LVER.

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- An automatic Vicat apparatus was used to determine the setting times of AAS pastes. The initial setting times of AAS pastes were determined when the needle penetration depth reached 6 ± 3 mm according to EN196-3 standard [21].
- 155

156 *2.3.4 Heat evolution of AAS pastes*

The calorimetric curves of AAS pastes were measured by eight-channel isothermal calorimetry (TA
instrument, USA). After mixing, the AAS pastes were immediately placed into a glass ampoule;
afterward, the ampoule was sealed and loaded into the isothermal calorimetry. The calorimetric
measurements were carried out at a temperature of 20 °C for 3 days.

161

162 2.3.5 ¹H-²⁹Si solid-state cross-polarization magic angle spinning nuclear magnetic resonance

163 (CPMAS NMR) and ²⁹Si MAS NMR analysis

164 It is important to select an appropriate technique to stop the reactions prior to ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR tests. In this study, the method to arrest the hydration of AAS was followed by 165 166 Chen et al. [23]. Firstly, the fresh pastes were mixed with deionized water and then subjected to 167 centrifugation to remove the liquid. This water extraction was repeated two times to remove the 168 soluble silicate species. Afterwards, a chemical extraction was carried out in a way that the solid part 169 was put on the 0.2 µm nylon filter membrane, and then at least 400 ml solvent (50/50 volume of 170 methanol/acetone) was added to wash the solid part and remove the water. Before NMR analysis, the 171 residual particles were collected and stored in a mild vacuum condition for 24 hours. Palacios et al. 172 [12] also noted that the initial washing of the AAS pastes with water and subsequent treatment with 173 isopropanol also can be an appropriate method to achieve the stoppage reactions in AAS pastes.

174

¹H-²⁹Si solid-state CPMAS NMR and ²⁹Si MAS NMR spectra were acquired on an Agilent VNMRS
Direct Drive 400 MHz spectrometer (9.4 Tesla) equipped with a T3HX 3.2 mm probe. The signal of
talc for both two types of NMR tests was used to calibrate the silicon chemical shift scale (-98 ppm).
Magic angle spinning was performed at 8 kHz and 6.5 kHz using ceramic zirconia rotors for ¹H-²⁹Si
CP MAS NMR and ²⁹Si MAS NMR test, respectively. Acquisition parameters in ¹H-²⁹Si CP MAS

180 NMR (or ²⁹Si MAS NMR) used were: a spectral width of 24 kHz, a 90° pulse length of 3.2 μ s (or 4.5 181 μ s), an acquisition time of 15 ms, a recycle delay time of 3 s (or 20 s), a spin-lock field of 80 kHz, a 182 contact time of 1 ms (or a recycle delay time of 20 s), and about 100000 accumulations (or about 8000 183 accumulations). High-power proton dipolar decoupling during the acquisition time for both two types 184 of NMR tests was set to 80 kHz. The spectra of ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR were 185 decomposed by the Gaussian peaks, and the specified full width at half height was always less than 10 186 ppm [24].

187

188 2.3.6 Scanning electron microscopy of AAS pastes

189 SEM with secondary electron mode were used to observe the morphology of AAS pastes. The

190 stoppage method of the reactions was elucidated in the previous section. The specimens at different

191 reaction times were carbon coated before imaging.

192

3. Results and discussions

194 *3.1 Structural build-up behavior and initial setting times of AAS pastes.*

195 Fig. 3a presents the evolution of the early storage modulus of AAS pastes activated by sodium 196 hydroxide and sodium silicate. As seen in Fig. 3a, these two mixtures exhibited completely different 197 structural build-up behavior. The increase of structural build-up of sodium hydroxide-activated slag 198 paste started off with a greater storage modulus, followed by a steadily rising rate of structural build-199 up over time. The trend of the structural build-up behavior is quite similar to that of Portland cement. 200 Previous studies have reported that a sharp increase in the storage modulus is observed in the first 30 201 min for Portland cement due to the formation of the percolated network [9], [10], [25]. After that, the 202 storage modulus increases at a relatively lower rate, indicating the sequential development of 203 hydration products at cement particle contact locations [9]. Due to the high alkaline environment for 204 the mixture NH-AAS, the rapid reaction rate of GGBFS could also enhance the formation of reaction 205 products, furthermore inducing the occurrence of the percolated network [6]. In the meantime, the 206 rapid reaction product formation could cover slag's surface, preventing further slag reaction [7].

Therefore, a continuous increase in the storage modulus of NH-AAS could be observed. It could then
be considered that the setting process of NH-AAS follows a similar mechanism as that of Portland
cement [20].

210

211 However, the evolution of the structural build-up of SS-AAS was significantly different from the case 212 of NH-AAS. The initial storage modulus started from a very low value as compared to NH-AAS. In 213 the first 20 min, almost no structural formation could be observed for the mixture SS-AAS. However, 214 afterwards, the storage modulus of SS-AAS steeply increased. Some researchers attribute the very low 215 initial storage modulus of SS-AAS to the viscous nature of sodium silicate solution with a great 216 number of aqueous silicates, which prevents the formation of the percolated network [10], [26]. The 217 mild alkaline environment provided by the sodium silicate solution allowed a considerable time to 218 dissolve GGBFS, providing sufficient calcium and aluminum. Once these ions reach their critical 219 concentration, they will interact with the silicates originated from the activator solution, significantly 220 leading to a significantly larger number of reaction products in the matrix [7], [10], [12]. Therefore, a 221 rapid increase in storage modulus could be observed for the SS-AAS mixtures. It should be noted here 222 that the initial setting times of AAS pastes were also consistent with the trend of the structural build-223 up. The mixture of SS-AAS showed a short initial setting (45 min) as compared to that of NH-AAS 224 (120 min).

225

Fig. 3b presents the evolution of loss factor of NH-AAS and SS-AAS mixture. In first 20 min, the loss
factor for NH-AAS mixture decreased dramatically, afterwards, the downward trend started to slow
down until the loss factor dropped to 0, reflecting that the paste reached solid-like state at around
initial setting time (120 min). By contrast, mixture SS-AAS showed an inverse trend. The loss factor
for mixture SS-AAS decreased slowly in the first 20 min, indicating its more viscous behavior. Then,
a rapid decrease could be observed for SS-AAS mixture until its initial setting time (45 min). This
showed that SS-AAS mixture reached solid-like state earlier than NH-AAS mixture.



Fig. 3. Evolution of storage modulus (a) and loss factor (b) of sodium hydroxide-activated and sodium silicateactivated GGBFS pastes.

234

238 *3.2 Calorimetric investigation of AAS pastes.*

239 The evolution of calorimetric curves, including heat flow and cumulative heat release of AAS pastes, 240 is presented in Fig. 4. As well known, there are five distinct stages for the AAS mixtures: dissolution, 241 induction, acceleration, deceleration and steady-state [29]-[32]. As demonstrated in Fig. 4a, the AAS 242 mixtures exhibited a high local peak during the first 20 min. Rapid heat evolution was observed when 243 the activator solution was in contact with GGBFS, being mostly related to the wetting and dissolution 244 of GGBFS particles and partly related to the interaction of silicate units and sodium with calcium and 245 aluminum dissolved from GGBFS [33], [34]. For SS-AAS pastes, the dissolution stage was followed 246 by an induction period in the heat flow, while no such period was seen for the NH-AAS pastes. The 247 observed acceleration peak (second peak) after the induction period for the AAS pastes is usually 248 associated with the onset of the main strength and microstructural development [35]. The occurrence 249 of the acceleration peak of SS-AAS was delayed as compared to the NH-AAS mixture, and the 250 intensity of the acceleration peak in the SS-AAS was lower as compared to the NH-AAS mixture, 251 which is also consistent with previous studies [29], [33]. This could be related to the lower pH value of 252 the sodium-silicate activator solution compared to the sodium-hydroxide activator (Table 2). It was 253 reported that the higher alkaline environment normally enhances the dissolution rate and slag reaction 254 degree [36]. Additionally, increasing alkalinity also improves the solubility of silica and alumina in 255 solution, which could induce more reaction product formation [27], [37].

The cumulative heat release of NH-AAS showed a higher value as compared to that of SS-AAS at the age of 72 h. However, in the first 3.5 h, the SS-AAS released more heat than NH-AAS. This is probably due to the interaction between the calcium ions, continuously released from GGBFS, and the silicate ions, originating from sodium silicate solution, quickly forming large amounts of gel products [38]. This is also consistent with the rapid increase in storage of SS-AAS in the early time. On the other hand, NH-AAS and SS-AAS both presented a similar cumulative heat release of around 17 J/g at





Fig. 4. Evolution of heat flow (a) and cumulative heat release (b) of sodium hydroxide-activated and sodium
 silicate-activated GGBFS pastes.

267

264

268 *3.3 NMR analysis of AAS pastes*

269 To further understand the relationships between the nanostructure and the setting process of AAS, 270 NMR tests were carried out on the samples taken at critical reaction times based on storage modulus, 271 setting time and calorimetric measurements. Three samples were taken at 20 min and 45 min (initial 272 setting time, as shown in Table 2) for the SS-AAS mixture and at 120 min (initial setting time) for the 273 NH-AAS mixture based on storage modulus and setting times as shown in Fig. 3. In addition, two 274 samples were taken from the SS-AAS mixture corresponding to the beginning of the acceleration stage 275 (16 h) and the end of the deceleration period (72 h), based on the calorimetry measurements as shown 276 in Fig. 4.

277

278 *3.3.1 NMR analysis at initial setting times*

279 The ²⁹Si MAS NMR spectra of the anhydrous GGBFS and the pastes at different reaction times are

given in Fig. 5. As shown in Fig. 5, the anhydrous slag was the primary source of the signal at -76.8

ppm in all the spectra. In addition, a shoulder between -80 and -105 ppm was observed at the initial

- setting time for NH-AAS (120 min) and SS-AAS mixtures (45 min), reflecting the reaction product
- formation. Therefore, these reaction products should be responsible for the initial setting of AAS. No

difference was observed between the spectra of SS-AAS_20min and anhydrous GGBFS, indicating no

- reaction product formation at 20 min. This was also consistent with the results of the structural build-
- up of the SS-AAS mixture, showing no significant structural formations at 20 min.
- 287

To better understand the nanostructure of AAS, an accurate deconvolution should be performed on the shoulder region. However, since some Qⁿ (mAl) (n=0,1,2,3,4 and m=0,1,2,3,4) peaks were overlapped in the ²⁹Si MAS NMR spectra [39], a ¹H-²⁹Si CPMAS NMR test was performed to find the peak positions, prior to the deconvolution of ²⁹Si MAS NMR spectra. It should be noted that the chemical shift of each resonance is required to be consistent in both the ²⁹Si MAS NMR and ¹H-²⁹Si CPMAS NMR spectral deconvolutions.

294

Fig. 6 and Fig. 7 present the differences between the ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR 295 spectra of the pastes activated by sodium hydroxide and sodium silicate, respectively, as well as their 296 detailed deconvolution. The resonances observed in the ¹H-²⁹Si CPMAS NMR are influenced by their 297 298 proximity to protons and the Hartmann-Hahn contact period, and so this spectrum particularly shows 299 those Si species present in the hydration reaction products [40]. As a result, the ¹H-²⁹Si CPMAS NMR data in Fig. 6 and 7 can confirm that the broad resonance feature observed in the ²⁹Si MAS NMR is 300 301 highly due to the presence of the anhydrous slag in the AAS. It should be noted that although the ¹H-302 ²⁹Si CPMAS NMR can provide better resolution of the spectra in terms of reaction products, it can 303 only give qualitative information rather than quantitative information. Therefore, the combined use of 304 ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR enables a more complete examination of the variations in 305 the nanostructure of reaction products that are formed in the AAS mixtures.

307	The nanostructure of AAS can be identified by the Q ⁿ (mAl) structural units, showing various chemical
308	environments of silicon tetrahedral of phases in ²⁹ Si NMR spectra, where n denotes the number of
309	oxygen bridges between each silicon tetrahedral unit and other silicon atoms, and m represents the
310	number of aluminum tetrahedral occupying bridging positions [41], [42]. The deconvolution results of
311	the Q ⁿ (mAl) structural units in the ²⁹ Si MAS NMR spectra are summarized in Table 3. The
312	deconvoluted peak located around -76.8 ppm for NS-AAS and SS-AAS mixtures at initial setting
313	times refers to the remnant GGBFS (Q^0), and the integration of these peaks reached 80.04% and 81.28%
314	of the spectra of ²⁹ Si MAS NMR, respectively. In other words, when both NH-AAS and SS-AAS
315	mixtures show an initial setting, they both have a similar reaction degree. Therefore, it may indicate
316	that the initial setting of AAS would occur when the reaction degree of GGBFS approached 20%.
317	Combining the results of rheology and setting time, it can be concluded that the solidification of NH-
318	AAS is a continuous process; however, the initial set of SS-AAS occurs suddenly in a shorter period
319	[20].
320	

321 As shown in Fig. 6b, the peak position for the mixture NH-AAS 120 min with $\delta = -79.2$ is attributed 322 to the Q¹ site, which is a terminal silicate tetrahedral site inside C-A-S-H gels [24], [43]. The middle-323 of-chain silicate inside C-A-S-H gels is connected to the Q²(1Al) and Q² sites at -83.5 ppm and -86 324 ppm, respectively [41], [44]. Since there is an overlap between resonances in this region, the peak at -325 89.2 ppm belongs to Q³(1Al) and Q⁴(4Al) sites [16], [24], [45]. Herein, it should be noted that the 326 Q³(1Al) site denoted a substantial degree of cross-linking with the C-(N-)A-S-H gel [24], [40], while Q⁴(4Al) site refers to the Al-rich N-A-S-H gel [46]. Additionally, Q⁴(2Al), Q⁴(1Al), and Q⁴(0Al) each 327 328 have their own set of three extra sites located somewhere in the range of -96 to -110 ppm. The Q⁴(mAl) 329 environments are attributed to a polymerized Si-rich N-A-S-H gel [12], [40], [47]. 330

331 Similarly, as shown in Fig. 7b, three resonances with $\delta = -78.5$ ppm, -83.0 ppm and -86 ppm, are

attributed to Q^1 , $Q^2(1Al)$ and Q^2 sites, respectively, indicating the formation of C-A-S-H in the SS-

333 AAS mixture. The $Q^{3}(1Al)$ and $Q^{4}(4Al)$ sites are located at -88.6 ppm, showing the formation of high

crosslinking C-(N-)A-S-H and N-A-S-H, respectively. In addition, the alumino-silicate gel N-A-S-H
can be confirmed by three additional peaks between -93 and -106 ppm, indicating the Q⁴(3Al), Q⁴(2Al)
and Q⁴(1Al) sites, respectively.

337

As shown in Table 3, it is found that the SS-AAS mixture showed a higher percentage of N-A-S-H 338 formation (Q⁴(mAl)) as compared to C-A-S-H (Q¹, Q²(1Al) and Q²), while the amount of C-A-S-H 339 340 (Q¹, Q²(1Al) and Q²) was more than N-A-S-H (Q⁴(mAl)) in the NH-AAS mixture. Although it was 341 very difficult to distinguish the net amounts of $Q^3(1AI)$ and $Q^4(4AI)$ due to their overlapped resonance, 342 it could still be concluded that the SS-AAS mixture contained a higher percentage of N-A-S-H as 343 compared to the NH-AAS mixture at initial setting times based on the other Q species. In addition, it is 344 well known that the sodium silicate solution contains high Q species [13], [17]. Due to the condensed 345 silicates in the activator of SS-AAS, these higher-Q Si species are more likely to condense with Al and 346 Ca to form 3D Ca-modified gel at early ages [48], [49]. While regarding the NaOH-activated mixture, 347 congruent dissolution of the various Si coordination environments in the precursors is highly unlikely 348 to occur during alkali activation due to the presence of many phases in the precursors and the 349 previously observed preference of Al over Si dissolution in the silicoaluminate precursors. 350 Furthermore, the highly polymerized aluminosilicate phase is predicted to disintegrate more slowly 351 than the depolymerized calcium silicate phases observed in the precursors [46], [50]. And these 352 released depolymerized silicates interacted with aluminum and calcium ions to form chain-like C-A-S-353 H gel [15], [37]. This could be the reason for the distinctive difference between SS-AAS and NH-AAS 354 in terms of gel composition at early ages.

355

It is plausible to see that the hydration products of AAS at initial setting times are composed of the CA-S-H and N-A-S-H gels. In the meantime, the coexistence of C-A-S-H and N-A-S-H resulted in a 3D
Ca-modified gel (N,C)-A-S-H, which was also reported by Garcia-Lodeiro et al. [51]. However, very
few studies have focused on the gel composition of AAS at the initial setting time in the literature.
Only Palacios et al. [12] used the thermodynamic modeling and NMR technique to confirm the
presence of the coexisting formation of the alumino-silicate gel and C-A-S-H gel in the sodium

362 silicate-activated slag mixtures at early times. These C-A-S-H and N-A-S-H gels are formed from the 363 reactions of Ca^{2+} ions and aluminate species dissolved from slag and Na⁺ and silicate species initially 364 existed in the solution. Therefore, the rheological properties and the setting process are determined by 365 these reaction products.

366

367 However, many studies, in general, pointed out that the main reaction products of AAS at later ages 368 are C-A-S-H gels. It is, therefore, very worthwhile to investigate when these N-A-S-H gels start to 369 disappear or whether they are converted into C-A-S-H gels as the reaction continues. Therefore, to 370 investigate a possible change in the gel composition of AAS at an early time, NMR tests were 371 conducted on the samples taken at two critical reaction times based on the isothermal calorimetric 372 curves of SS-AAS pastes (as shown in section 3.4.2).

373



Fig. 5. The original ²⁹Si MAS NMR spectra of AAS, (a) NH-AAS, (b) SS-AAS.



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- 378



Fig. 6. The deconvolution of ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR spectra of NH-AAS at initial setting
 time (120 min), (a) The deconvolution of ¹H-²⁹Si CPMAS NMR, (b) The deconvolution of ²⁹Si MAS NMR.





Fig. 7. The deconvolution of ¹H-²⁹Si CPMAS NMR and ²⁹Si MAS NMR spectra of SS-AAS at the initial setting
time (45 min), (a) The deconvolution of ¹H-²⁹Si CPMAS NMR, (b) The deconvolution of ²⁹Si MAS NMR.

Mixtures	Unreacted	Reaction Products									
	slag										
		C-A-S	5-H/C-(N-)	A-S-H		N-A-S-H					
	Q^0	Q ¹	Q^1 $Q^2(1Al)$		Q ³ (1Al)	Q ⁴ (3Al)	Q ⁴ (2Al)	Q ⁴ (1Al)	Q ⁴ (0Al)		
					&Q4(4Al)						
NH-	80.04	4.93	2.74	1.34	4.38	-	4.59	1.62	0.38		
AAS_120min	(-76.8	(-78.5	(-83.0	(-86.4	(-89.3		(-96.5	(-104.4	(-110.4		
	ppm)	ppm)	ppm)	ppm)	ppm)		ppm)	ppm)	ppm)		
SS-	81.28	1.07	1.93	1.51	5.32	2.99	4.75	1.14	-		
AAS_45min	(-76.8	(-78.5	(-83.1	(-86.0	(-89.0	(-93.1	(-97.2	(-105.6			
	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)			
SS-AAS_16h	68.68	2.45	3.80	4.65	7.63	5.34	4.85	2.60	-		
	(-76.8	(-78.5	(-83.1	(-86	(-88.9	(-93.1	(-97.3	(-105.6			
	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)			
SS-AAS_72h	48.46	18.22	13.58	8.09	5.55	3.68	2.42	-	-		
	(-76.8	(-78.8	(-83.6	(-86.2	(-89.1	(-93.6	(-97.5				
	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)	ppm)				

395 Table 3. The deconvolution results of the ²⁹Si MAS NMR spectra of AAS mixtures over time based on area

396 percentage (%).

398

399 3.3.2 NMR analysis of SS-AAS pastes based on calorimetric curves

Fig. 8 illustrates the ²⁹Si MAS NMR of SS-AAS pastes over time. As the curing age increased from the beginning to 16 h, the broad peak did not shift significantly, while the shoulder area between -80 and -105 ppm was enhanced. With time elapsing from 16 h to 72 h, the broad peak started to shift to a higher value, and the shoulder area between -90 and 105 ppm significantly decreased. This is possibly due to the increase of polymerization degree and cross-linking of gels over time and the disappearance of the alumino-silicate gel.

407 ²⁹Si MAS NMR decomposition results of the SS-AAS mixture at around the starting time of the 408 acceleration peak and the end of the deceleration peak observed in the isothermal calorimetric curves 409 are presented in Fig. 9. The area percentage of various Qn(mAl) structural units are quantified and 410 summarized in Table 3. As can be seen from Fig. 9, $Q^2(1AI)$ and Q^2 sites within C-A-S-H increased 411 from 3.80 % to 13.58 % and from 4.65 % to 8.09 % with increasing curing time from 16 h to 72 h, 412 respectively. In particular, the content of Q¹ significantly increased from 2.45 % to 18.22 % with time 413 elapsing and became the most dominant Qⁿ(mAl) structural unit in SS-AAS pastes at the age of 72 h. 414 This is also consistent with the previous studies, reporting the dissolved calcium and aluminum from 415 slag enhance the gel polymerization and result in more crosslinked C-A-S-H gels [24]. During the 416 proceeded reaction time from the initial setting time (45 min) to 16 h and then to 72 h, the content of 417 $Q^{3}(1AI) \& Q^{4}(4AI)$ gradually increased from 5.32 % to 7.63 % and then decreased to 5.55 %. 418 Meanwhile, the content of N-A-S-H gel (including Q⁴(mAl), m=3, 2, 1, 0) first increased from 8.88 % 419 to 12.79 % when the age increased from 45 min to 16 h and then decreased to 6.10 % when the age 420 increased from 16 h to 72 h. This indicates that the system is continuously enriched with N-A-S-H 421 until the end of the induction period; however, as the reaction proceeded, the N-A-S-H started to 422 destabilize to form C-A-S-H when reaching the end of the second exothermic peak of SS-AAS. 423 424 Based on the NMR results in this study and the compatibility between C-A-S-H and N-A-S-H gels 425 [51], the activation process of SS-AAS pastes in the early times can be explained as follows. After 426 mixing the GGBFS with sodium silicate solution, the process begins with the dissolution of the 427 GGBFS particles in the alkaline solution via rupture of the T-O-T bonds (T: Si or Al) and Ca-O bonds 428 in the slag, resulting in a wide variety of dissolved species. This can be confirmed by various previous 429 studies, which use ICP-OES to observe the change of different ion concentrations [6], [7], [13], [15], 430 [27], [37]. When the ions reach their oversaturation, a great number of C-A-S-H and N-A-S-H gels 431 precipitate. These gels generally contain a high aluminum content, as shown in the NMR results in this 432 study. As the alkaline reaction proceeds, the silicates from the original activator solution are consumed

433 during the formation of reaction products. Therefore, the Si-O bonds in GGBFS start to dissolve and

434 keep the silicon concentration at a high level. In this study, from the initial setting time to 16 h, Si

uptake enhances the gel condensation in terms of C-A-S-H, leading to an increase in Q²(1Al). In the
meantime, the percentage of N-A-S-H gel also increases when the age increases from the initial setting
time to 16 h.

438

439 Additionally, with time elapsing, the calcium and aluminum ions in the aqueous solution begin to 440 diffuse throughout the cementitious matrix and a certain level of Ca ions reacts with N-A-S-H to form 441 (N,C)-A-S-H. Since calcium and sodium ions have the same ionic radius and electronegative potential, 442 the 3D structure of the (N,C)-A-S-H type gel is maintained by an ion exchange process, in which 443 calcium can replace the sodium ions in a mechanism similar to that observed in clay and zeolites [52]. 444 When calcium concentrations are high enough, they diffuse into pores in the matrix and interact with 445 the (N,C)-A-S-H gel. Because of the Ca²⁺ polarising effect, the Si-O-Al bonds are under tension and 446 eventually broken, forming Si-O-Ca bonds. As aluminum is released from the N-A-S-H gel, fewer 447 polymerized structures, such as C-A-S-H gels, are formed. Simultaneously, the C-A-S-H gel formed in 448 earlier phases is capable of absorbing a significant amount of silicon and aluminum ions in bridge 449 positions [53]. Besides, Puertas et al. [15] also found that the calcium concentration and pH value of 450 the waterglass-activated slag mixtures reached a peak value at the age of 24h. This also supports that 451 the N-A-S-H gel will degrade to C-A-S-H due to its low stability in the presence of high pH and high 452 calcium concentrations, as reported by Garcia-Lodeiro et al. [51]. Eventually, the chain-like C-A-S-H 453 gels will form and dominate the reaction products, which is also consistent with this study where O^1 454 Q^2 and $Q^2(1Al)$ are the main Q species at the age of 72h.





Fig. 8. The ²⁹Si MAS NMR spectra of anhydrous GGBFS and SS-AAS pastes at different times.





459 Fig. 9. The deconvolution of ²⁹Si MAS NMR spectra of SS-AAS at around: (a) starting point of the acceleration
460 period (16 h) and (b) at the end of the deceleration period (72 h) based on isothermal calorimetric curves.

461

462 3.3.3 Quantitative assessment of C-A-S-H/C-(N-)A-S-H and N-A-S-H

Fig. 10 presents the deconvolution results for the ²⁹Si MAS NMR spectra of the SS-AAS mixture over time.

464 It could be seen that in the first 16 h, the $Q^4(mAl)$ is dominated as compared to other Q^n environments. As curing

465 time proceeded, the $Q^4(mAl)$ started to decrease, in particular for the $Q^4(1Al)$, which decreased to zero at 72 h.

- 466 However, other chain-like Q^n increased.
- 467



- 468
- 469

Fig. 10. The deconvolution results for the ²⁹Si MAS NMR spectra of SS-AAS mixture over time.

470

471 Richardson and Groves [54] have proposed a conceptual model named "substituted general model" (SGM) to

describe the C-(N-)A-S-H product, which is a mixture of 14 Å tobermorite, jennite, and Ca(OH)₂ structures.

473 However, in recent studies, more formation of cross-linked Si sites, such as Q³ and Q³(1Al), is identified by the

474	high-resolution ²⁹ Si MAS NMR [24], [36], [39], [41]. As reported by Myers et al. [24], in tobermorite structural
475	models, Q3-type silica bonding environments can only be described by cross-linking between bridging sites in
476	the silicate chains. Therefore, another conceptual model, the "Cross-linked substituted tobermorite model"
477	(CSTM), has been proposed to support the description of the C-(N-)A-S-H gel as a mixture of cross-linked (11 Å
478	tobermorite) and non-cross-linked (14 and/or 9 Å tobermorite) chains. And it should be noted that there are some
479	structural constraints included in the CSTM model: (i) two times as many silicate species exist in the form (Q^2 +
480	$Q^{2}(1Al)$) as in the form ($Q^{3} + Q^{3}(1Al) + Al[4]$). (ii) since aluminum is only substituted into bridging sites in
481	cross-linked tobermorite, the fraction of aluminum substitution into Q^3 type sites is equal to the ratio of $Q^2(1Al)$
482	to Q ² sites, and (iii) the introduction of one Al[4] species into cross-linked tobermorite introduces one Q ³ (1Al)
483	and two Q ² (1Al) Si species. Regarding the structure of N-A-S-H, unfortunately, no acknowledged conceptual
484	model has been proposed due to its complicated 3D structures.
485	
486	To further investigate the structure of the investigated samples in this study, two extreme scenarios are
487	considered. In this study, as the $Q^{3}(1Al)$ and $Q^{4}(4Al)$ are overlapped at around -89 ppm, it was assumed as a first
488	case that all the signals came from $Q^4(4Al)$ and there was no $Q^3(1Al)$ in the nanostructure, which means all C-
489	(N-)A-S-H structures consist of non-cross-linked gel as defined by the SGM model. In the second extreme case,
490	it was assumed that the C-(N-)A-S-H had the maximum crosslinking degree (maximum content of Q ³ (1Al), and
491	the remaining part is $Q^4(4Al)$), considering the abovementioned structural constraints. This indicates that the C-
492	(N-)A-S-H is a mixture of cross-linked and non-cross-linked tobermorite-like structures as defined by CSTM.
493	
494	Table 4 presents the C-A-S-H/C-(N-)A-S-H and N-A-S-H gel amounts considering the two extreme scenarios
495	above. As shown in Table 4, the calculated amounts of C-A-S-H/C-(N-)A-S-H and N-A-S-H vary in a narrow
496	band for these two extreme scenarios except the mixture SS-AAS_72h. For example, NH-AAS_120 min
497	exhibited a range of C-A-S-H/C-(N-)A-S-H between 9.01 and 9.68, and N-A-S-H was between 10.30 and 10.97.
498	In both scenarios, the relative amount of C-A-S-H/C-(N-)A-S-H is closer to N-A-S-H gel for the mixture of NH-
499	AAS_120 min, while the N-A-S-H gel is much more dominant in the mixture of SS-AAS_45 min. With time
500	elapsing, the C-A-S-H/C-(N-)A-S-H amount increased rapidly, while the amount of N-A-S-H firstly increased
501	until the end of the induction period based on calorimetric curves. At the end of deceleration period based on
502	calorimetric curves (72h), the N-A-S-H formation for mixture SS-AAS decreased significantly for both two
503	extreme scenarios as compared to the mixture at the age of 16h.

	Mixture	Q ¹	Q ² (1Al)	Q^2	Q ³ (1Al)	Q4(4Al)	Q ⁴ (3Al)	Q4(2Al)	Q4(1Al)	Q4(0Al)	C-A-S-	N-A-
											H/C-(N-	S-H
)A-S-H	
No cross-link in	NH-											
C-A-S-H/C-(N)-	AAS_120min	4.93	2.74	1.34	-	4.38	-	4.59	1.62	0.38	9.01	10.97
A-S-H	SS-											
	AAS_45min	1.07	1.93	1.51	-	5.32	2.99	4.75	1.14	-	4.51	14.20
	SS-AAS_16h	2.45	3.80	4.65	-	7.63	5.34	4.85	2.60	-	10.90	20.42
	SS-AAS_72h	18.22	13.58	8.08	-	5.55	3.68	2.42	-	-	39.88	11.65
Maximum cross-	NH-											
link in C-A-S-	AAS_120min	4.93	2.74	1.34	0.67	3.71	-	4.59	1.62	0.38	9.68	10.30
H/C-(N)-A-S-H	SS-											
	AAS_45min	1.07	1.93	1.51	0.27	5.05	2.99	4.75	1.14	-	4.78	13.93
	SS-AAS_16h	2.45	3.80	4.65	0.61	7.02	5.34	4.85	2.60	-	11.51	19.81
	SS-AAS_72h	18.22	13.58	8.08	4.04	1.51	3.68	2.42	-	-	43.92	7.61

504 Table 4 Nanostructure of investigated pastes in this study considering the two extreme scenarios.

506 3.4 SEM images of AAS pastes

507 Scanning electron microscopy (SEM) was used to evaluate the surface morphology development of

the AAS pastes [12], [16]. Fig. 13 presents SEM images of AAS pastes during the reaction process. At

the age of 120 min for NH-AAS (Fig. 13c and 13d) and 45 min for SS-AAS (Fig. 13g and 13h), the

510 GGBFS particle surfaces became rough due to the precipitation of reaction products, thereby probably

511 leading to the initial set of AAS pastes.

512

513 As shown in Fig. 13e and 13f, the surface of the GGBFS particles of the SS-AAS mixture at the age of

514 20 min was very smooth, indicating no detectable reaction product formation at this age. This is also

515 consistent with the structural build-up and NMR results in this study. With time elapsing, the

516 dissolved calcium and aluminum ions from the GGBFS reached oversaturation and interacted with the

517 silicates originating from the activator solution, forming more reaction products. Therefore, the surface

518 of GGBFS particles became increasingly rough, and more particles would connect to each other due to

the formation of reaction products (as shown in Fig. 13k and 13l) [12].



Original GGBFS



NH-AAS_120min



SS-AAS_20min



SS-AAS_45min



SS-AAS_16h



- Fig. 13. SEM images of AAS pastes over time; (a, b) anhydrous GGBFS; (c, d) NH-AAS at 120 min; (e, f) SS-

AAS at 20 min; (g, h) SS-AAS at 45 min; (i, j) SS-AAS at 16 h; (k, l) SS-AAS at 72 h.

538 **4.** Conclusions

539 Following are the primary conclusions that can be derived from the experimental findings:

The NH-AAS reaches its initial setting time with a long, continuously proceeding 540 541 structuration process. On the contrary, SS-AAS reaches its initial setting with an abrupt 542 increase in the structuration process. At their initial setting times, the NH-AAS and SS-AAS 543 mixtures release similar heat and reach a similar reaction degree. 544 • At initial setting times, the C-A-S-H and N-A-S-H gels are both formed in the NH-AAS and SS-AAS mixtures. The difference, however, is that the amount of C-A-S-H gel is relatively 545 546 similar to N-A-S-H gel in NH-AAS, while SS-AAS contains much more N-A-S-H gel. 547 • With time elapsing, more N-A-S-H gel in the SS-AAS mixture precipitates up to the end of 548 the induction period. However, the 3D N-A-S-H gel degrades to a chain-like C-A-S-H gel 549 after the acceleration peak recorded in the isothermal calorimetric curves. 550 551 The findings presented in this study can help researchers understand, to some extent, the early gel

552 composition and alkaline activation process of AAS mixtures. However, some remaining challenges

still need to be addressed in further research. For example, modeling the N-A-S-H structure could help

understand the reaction process. In addition, more research on the relationships between the

555 composition factors and inter-particle forces could also help better understand the interaction

556 mechanisms before setting times.

557

558 Authorship contribution statement

Xiaodi DAI: Methodology, Conceptualization, Investigation, Writing – original draft; Serdar
AYDIN: Methodology, Conceptualization, Writing – review editing; Mert Yücel YARDIMCI:
Methodology, Validation, Writing – review editing; Gunter REEKMANS: Investigation, Validation;
Peter ADRIAENSENS: Investigation, Validation; Geert De SCHUTTER: Funding acquisition,
Supervision, Writing - review & editing.

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571

572 **Reference**

- 573 [1] RILEM-TC 224-AAM, Alkali Activated Materials. 2014.
- 574 [2] J. L. Provis and S. A. Bernal, "Geopolymers and Related Alkali-Activated Materials," *Annu. Rev. Mater.*575 *Res.*, vol. 44, no. 1, pp. 299–327, 2014, doi: 10.1146/annurev-matsci-070813-113515.
- 576 [3] C. Shi, B. Qu, and J. L. Provis, "Recent progress in low-carbon binders," *Cem. Concr. Res.*, vol. 122, no.
 577 May, pp. 227–250, 2019, doi: 10.1016/j.cemconres.2019.05.009.
- 578 [4] S. K. Nath and S. Kumar, "Reaction kinetics, microstructure and strength behavior of alkali activated
 579 silico-manganese (SiMn) slag Fly ash blends," *Constr. Build. Mater.*, vol. 147, pp. 371–379, 2017, doi:
- 580 10.1016/j.conbuildmat.2017.04.174.
- 581 [5] S. A. Bernal and J. L. Provis, "Durability of alkali-activated materials: Progress and perspectives," *J. Am.*582 *Ceram. Soc.*, vol. 97, no. 4, pp. 997–1008, 2014, doi: 10.1111/jace.12831.
- 583 [6] X. Dai, S. Aydin, M. Y. Yardımcı, R. Qiang, K. Lesage, and G. De Schutter, "Rheology, early-age
- 584 hydration and microstructure of alkali-activated GGBFS-Fly ash-limestone mixtures," *Cem. Concr.*

585 *Compos.*, vol. 124, no. May, p. 104244, 2021, doi: 10.1016/j.cemconcomp.2021.104244.

- 586 [7] X. Dai, S. Aydın, M. Y. Yardımcı, K. Lesage, and G. De Schutter, "Effects of activator properties and
- 587 GGBFS/FA ratio on the structural build-up and rheology of AAC," *Cem. Concr. Res.*, vol. 138, no.
- 588 October, p. 106253, 2020, doi: 10.1016/j.cemconres.2020.106253.
- 589 [8] X. Dai, S. Aydin, M. Y. Yardimci, and G. De Schutter, "Rheology and structural build-up of sodium
 590 silicate- and sodium hydroxide-activated GGBFS mixtures," *Cem. Concr. Compos.*, vol. 131, Aug. 2022,
 591 doi: 10.1016/j.cemconcomp.2022.104570.
- 592 [9] N. Roussel, G. Ovarlez, S. Garraul, C. Brumaud, "The origins of thixotropy of fresh cement pastes,"
- 593 *Cem. Concr. Res.*, no. 42, pp. 148–157, 2012, doi: 10.1016/j.cemconres.2011.09.004.

- 594 [10] M. F. Alnahhal, T. Kim, and A. Hajimohammadi, "Distinctive rheological and temporal viscoelastic
 595 behaviour of alkali-activated fly ash / slag pastes : A comparative study with cement paste," *Cem. Concr.*
- **596** *Res.*, vol. 144, no. March, p. 106441, 2021, doi: 10.1016/j.cemconres.2021.106441.
- 597 [11] A. Kashani, J. L. Provis, G. G. Qiao, and J. S. J. Van Deventer, "The interrelationship between surface
 598 chemistry and rheology in alkali activated slag paste," *Constr. Build. Mater.*, vol. 65, pp. 583–591, 2014,
 599 doi: 10.1016/j.conbuildmat.2014.04.127.
- 600 [12] M. Palacios *et al.*, "Early reactivity of sodium silicate-activated slag pastes and its impact on rheological
 601 properties," *Cem. Concr. Res.*, vol. 140, no. July 2020, p. 106302, 2021, doi:
- **602** 10.1016/j.cemconres.2020.106302.
- 603 [13] N. Li, C. Shi, and Z. Zhang, "Understanding the roles of activators towards setting and hardening control
 604 of alkali-activated slag cement," *Compos. Part B Eng.*, vol. 171, no. January, pp. 34–45, 2019, doi:
 605 10.1016/j.compositesb.2019.04.024.
- 606 [14] W. Chen, B. Li, J. Wang, and N. Thom, "Effects of alkali dosage and silicate modulus on autogenous
 607 shrinkage of alkali-activated slag cement paste," *Cem. Concr. Res.*, vol. 141, no. February 2020, 2021,
 608 doi: 10.1016/j.cemconres.2020.106322.
- 609 [15] F. Puertas, A. Fernández-Jiménez, and M. T. Blanco-Varela, "Pore solution in alkali-activated slag
 610 cement pastes. Relation to the composition and structure of calcium silicate hydrate," *Cem. Concr. Res.*,
 611 vol. 34, no. 1, pp. 139–148, 2004, doi: 10.1016/S0008-8846(03)00254-0.
- 612 [16] I. Ismail, S. A. Bernal, J. L. Provis, R. San Nicolas, S. Hamdan, and J. S. J. Van Deventer, "Modification
 613 of phase evolution in alkali-activated blast furnace slag by the incorporation of fly ash," *Cem. Concr.*614 *Compos.*, vol. 45, pp. 125–135, 2014, doi: 10.1016/j.cemconcomp.2013.09.006.
- 615 [17] J. Aupoil, J. B. Champenois, J. B. d'Espinose de Lacaillerie, and A. Poulesquen, "Interplay between
 616 silicate and hydroxide ions during geopolymerization," *Cem. Concr. Res.*, vol. 115, no. May 2018, pp.
 617 426–432, 2019, doi: 10.1016/j.cemconres.2018.09.012.
- 618 [18] M. Nehdi and M. A. Rahman, "Estimating rheological properties of cement pastes using various
- 619 rheological models for different test geometry, gap and surface friction," *Cem. Concr. Res.*, vol. 34, no.
 620 11, pp. 1993–2007, 2004, doi: 10.1016/j.cemconres.2004.02.020.
- 621 [19] X. Dai, S. Aydin, M. Y. Yardımcı, and G. De Schutter, "Early Structural Build-up, Setting Behavior,
- 622 Reaction Kinetics and Microstructure of Sodium Silicate-Activated Slag Mixtures with Different
- 623 Retarder Chemicals," Cem. Concr. Res., vol. 159, p. 106872, 2022, doi:

- 624 10.1016/j.cemconres.2022.106872.
- 625 [20] X. Dai, S. Aydin, M. Y. Yardımcı, and G. De Schutter, "Rheology and structural build-up of sodium
- silicate- and sodium hydroxide-activated GGBFS mixtures," *Cem. Concr. Compos.*, vol. 131, no. May, p.
 104570, 2022, doi: 10.1016/j.cemconcomp.2022.104570.
- 628 [21] BS EN 196-3:2005 +A1:2008 Methods of testing cement Part 3: Determination of setting times and
 629 soundness, vol. 3, no. August. 2003.
- 630 [22] M. Ezzat, X. Xu, K. El Cheikh, K. Lesage, R. Hoogenboom, and G. De Schutter, "Structure-property
- relationships for polycarboxylate ether superplasticizers by means of RAFT polymerization," *J. Colloid Interface Sci.*, vol. 553, pp. 788–797, 2019, doi: 10.1016/j.jcis.2019.06.088.
- 633 [23] X. Chen, A. Meawad, and L. J. Struble, "Method to stop geopolymer reaction," *J. Am. Ceram. Soc.*, vol.
 634 97, no. 10, pp. 3270–3275, 2014, doi: 10.1111/jace.13071.
- 635 [24] R. J. Myers, S. A. Bernal, R. San Nicolas, and J. L. Provis, "Generalized structural description of
- 636 calcium-sodium aluminosilicate hydrate gels: The cross-linked substituted tobermorite model,"
- 637 *Langmuir*, vol. 29, no. 17, pp. 5294–5306, 2013, doi: 10.1021/la4000473.
- 638 [25] A. M. Mostafa and A. Yahia, "Physico-chemical kinetics of structural build-up of neat cement-based
 639 suspensions," *Cem. Concr. Res.*, vol. 97, pp. 11–27, 2017, doi: 10.1016/j.cemconres.2017.03.003.
- 640 [26] A. Favier, J. Hot, G. Habert, N. Roussel, and J. B. D'Espinose De Lacaillerie, "Flow properties of MK-
- based geopolymer pastes. A comparative study with standard Portland cement pastes," *Soft Matter*, vol.
- 642 10, no. 8, pp. 1134–1141, 2014, doi: 10.1039/c3sm51889b.
- 643 [27] Y. Zuo, M. Nedeljković, and G. Ye, "Pore solution composition of alkali-activated slag/fly ash pastes,"
 644 *Cem. Concr. Res.*, vol. 115, no. October 2018, pp. 230–250, 2019, doi:
- 645 10.1016/j.cemconres.2018.10.010.
- 646 [28] P. Perez-Cortes and J. I. Escalante-Garcia, "Gel composition and molecular structure of alkali-activated
 647 metakaolin-limestone cements," *Cem. Concr. Res.*, vol. 137, no. August, p. 106211, 2020, doi:
- 648 10.1016/j.cemconres.2020.106211.
- 649 [29] B. S. Gebregziabiher, R. Thomas, and S. Peethamparan, "Very early-age reaction kinetics and
- 650 microstructural development in alkali-activated slag," Cem. Concr. Compos., vol. 55, pp. 91–102, 2015,
- doi: 10.1016/j.cemconcomp.2014.09.001.
- 652 [30] X. Gao, Q. L. Yu, and H. J. H. Brouwers, "Properties of alkali activated slag-fly ash blends with
 653 limestone addition," *Cem. Concr. Compos.*, vol. 59, pp. 119–128, 2015, doi:

- 654 10.1016/j.cemconcomp.2015.01.007.
- K. Dai, S. Aydin, M. Y. Yardımcı, K. Lesage, and G. De Schutter, "Influence of water to binder ratio on
 the rheology and structural Build-up of Alkali-Activated Slag / Fly ash mixtures," *Constr. Build. Mater.*,
 vol. 264, p. 120253, 2020, doi: 10.1016/j.conbuildmat.2020.120253.
- 658 [32] X. Dai, S. Aydın, M. Y. Yardımcı, K. Lesage, and G. De Schutter, "Rheology and microstructure of
- alkali-activated slag cements produced with silica fume activator," *Cem. Concr. Compos.*, vol. 125, no.
 September 2021, p. 104303, 2022, doi: 10.1016/j.cemconcomp.2021.104303.
- 661 [33] X. Gao, Q. L. Yu, and H. J. H. Brouwers, "Reaction kinetics, gel character and strength of ambient
 662 temperature cured alkali activated slag-fly ash blends," *Constr. Build. Mater.*, vol. 80, pp. 105–115, 2015,
 663 doi: 10.1016/j.conbuildmat.2015.01.065.
- 664 [34] S. A. Bernal, "Effect of the activator dose on the compressive strength and accelerated carbonation
- resistance of alkali silicate-activated slag/metakaolin blended materials," *Constr. Build. Mater.*, vol. 98,
- 666 pp. 217–226, 2015, doi: 10.1016/j.conbuildmat.2015.08.013.
- 667 [35] C. Shi and R. L. Day, "A calorimetric study of early hydration of alkali-slag cements," *Cem. Concr. Res.*,
 668 vol. 25, no. 6, pp. 1333–1346, 1995.
- 669 [36] A. R. Brough and A. Atkinson, "Sodium silicate-based, alkali-activated slag mortars Part I. Strength,
 670 hydration and microstructure," *Cem. Concr. Res.*, vol. 32, no. 6, pp. 865–879, 2002, doi: 10.1016/S0008671 8846(02)00717-2.
- 672 [37] S. Song and H. M. Jennings, "Pore solution chemistry of alkali-activated ground granulated blast-furnace
 673 slag," *Cem. Concr. Res.*, vol. 29, no. 2, pp. 159–170, 1999, doi: 10.1016/S0008-8846(98)00212-9.
- 674 [38] R. Cao, S. Zhang, N. Banthia, Y. Zhang, and Z. Zhang, "Interpreting the early-age reaction process of
- alkali-activated slag by using combined embedded ultrasonic measurement , thermal analysis , XRD ,
- 676 FTIR and SEM," *Compos. Part B*, vol. 186, no. November 2019, p. 107840, 2020, doi:
- 677 10.1016/j.compositesb.2020.107840.
- 678 [39] F. Puertas, M. Palacios, H. Manzano, J. S. Dolado, A. Rico, and J. Rodríguez, "A model for the C-A-S-H
- 679 gel formed in alkali-activated slag cements," *J. Eur. Ceram. Soc.*, vol. 31, no. 12, pp. 2043–2056, 2011,
 680 doi: 10.1016/j.jeurceramsoc.2011.04.036.
- 681 [40] B. Walkley, X. Ke, J. L. Provis, and S. A. Bernal, "Activator Anion Influences the Nanostructure of
- Alkali-Activated Slag Cements," J. Phys. Chem. C, 2021, doi: 10.1021/acs.jpcc.1c07328.
- 683 [41] R. J. Myers, S. A. Bernal, J. D. Gehman, J. S. J. Van Deventer, and J. L. Provis, "The role of al in cross-

- 684 linking of alkali-Activated slag cements," *J. Am. Ceram. Soc.*, vol. 98, no. 3, pp. 996–1004, 2015, doi:
 685 10.1111/jace.13360.
- 686 [42] P. S. Singh, T. I. M. Bastow, M. Trigg, and C. S. Mdc, "Structural studies of geopolymers by 29 Si and
 687 27 Al MAS-NMR," vol. 0, pp. 3951–3961, 2005.
- 688 [43] X. Gao, Q. L. Yu, and H. J. H. Brouwers, "Apply 29 Si , 27 Al MAS NMR and selective dissolution in
 689 identifying the reaction degree of alkali activated slag- fly ash composites," *Ceram. Int.*, vol. 43, no.

690 May, pp. 12408–12419, 2017, doi: 10.1016/j.ceramint.2017.06.108.

- 691 [44] E. L. Hôpital, B. Lothenbach, G. Le Saout, D. Kulik, and K. Scrivener, "Incorporation of aluminium in
 692 calcium-silicate-hydrates," *Cem. Concr. Res.*, vol. 75, pp. 91–103, 2015, doi:
- **693** 10.1016/j.cemconres.2015.04.007.
- 694 [45] G. Fang and M. Zhang, "Multiscale micromechanical analysis of alkali-activated fly ash-slag paste,"
 695 *Cem. Concr. Res.*, vol. 135, no. May, p. 106141, 2020, doi: 10.1016/j.cemconres.2020.106141.
- 696 [46] B. Walkley et al., "Phase evolution of C-(N)-A-S-H/N-A-S-H gel blends investigated via alkali-
- 697 activation of synthetic calcium aluminosilicate precursors," *Cem. Concr. Res.*, vol. 89, pp. 120–135,
 698 2016, doi: 10.1016/j.cemconres.2016.08.010.
- 699 [47] G. Fang and M. Zhang, "Multiscale micromechanical analysis of alkali-activated fly ash-slag paste,"
 700 *Cem. Concr. Res.*, vol. 135, no. June, p. 106141, 2020, doi: 10.1016/j.cemconres.2020.106141.
- 701 [48] X. Chen, A. Sutrisno, and L. J. Struble, "Effects of calcium on setting mechanism of metakaolin-based
- 702 geopolymer," J. Am. Ceram. Soc., vol. 101, no. 2, pp. 957–968, 2018, doi: 10.1111/jace.15249.
- 703 [49] X. Chen, A. Sutrisno, L. Zhu, and L. J. Struble, "Setting and nanostructural evolution of metakaolin
 704 geopolymer," *J. Am. Ceram. Soc.*, vol. 100, no. 5, pp. 2285–2295, 2017, doi: 10.1111/jace.14641.
- 705 [50] B. Walkley, R. San, M. Sani, J. D. Gehman, J. S. J. Van Deventer, and J. L. Provis, "Synthesis of
 706 stoichiometrically controlled reactive aluminosilicate and calcium-aluminosilicate powders," *Powder*707 *Technol.*, vol. 297, pp. 17–33, 2016, doi: 10.1016/j.powtec.2016.04.006.
- 708 [51] I. Garcia-Lodeiro, A. Palomo, A. Fernández-Jiménez, and D. E. MacPhee, "Compatibility studies
- between N-A-S-H and C-A-S-H gels. Study in the ternary diagram Na2O-CaO-Al2O3-SiO 2-H2O,"
- 710 *Cem. Concr. Res.*, vol. 41, no. 9, pp. 923–931, 2011, doi: 10.1016/j.cemconres.2011.05.006.
- 711 [52] A. Palomo, D. E. Macphee, and A. Ferna, "Effect of Calcium Additions on N–A–S–H Cementitious
 712 Gels," vol. 1940, pp. 1934–1940, 2010, doi: 10.1111/j.1551-2916.2010.03668.x.
- 713 [53] I. G. Richardson, A. R. Brough, G. W. Groves, and C. M. Dobson, "The characterization of hardened

- 714 alkali-activated blast-furnace slag pastes and the nature of the calcium silicate hydrate (C-S-H) phase,"
- 715 *Cem. Concr. Res.*, vol. 24, no. 5, pp. 813–829, 1994, doi: 10.1016/0008-8846(94)90002-7.
- 716 [54] I. G. Richardson and G. W. Groves, "The incorporation of minor and trace elements into calcium silicate
 717 hydrate (C-S-H) gel in hardened cement pastes," *Cem. Concr. Res.*, vol. 23, pp. 131–138, 1993.
- 718 [55] W. Mozgawa and J. Deja, "Spectroscopic studies of alkaline activated slag geopolymers," J. Mol. Struct.,
- 719 vol. 924–926, no. C, pp. 434–441, 2009, doi: 10.1016/j.molstruc.2008.12.026.
- 720 [56] A. Fernandez-Jimenez and F. Puertas, "Structure of Calcium Silicate Hydrates Formed in Alkaline-
- Activated Slag : Influence of the Type of Alkaline Activator," *J. Am. Ceram. Soc.*, vol. 94, pp. 1389–
 1394, 2003.
- 723 [57] N. Li, N. Farzadnia, and C. Shi, "Microstructural changes in alkali-activated slag mortars induced by
 724 accelerated carbonation," *Cem. Concr. Res.*, vol. 100, no. July, pp. 214–226, 2017, doi:

725 10.1016/j.cemconres.2017.07.008.

- [58] I. García Lodeiro, D. E. Macphee, A. Palomo, and A. Fernández-Jiménez, "Effect of alkalis on fresh CS-H gels. FTIR analysis," *Cem. Concr. Res.*, vol. 39, no. 3, pp. 147–153, 2009, doi:
- 728 10.1016/j.cemconres.2009.01.003.
- 729 [59] S. Puligilla and P. Mondal, "Co-existence of aluminosilicate and calcium silicate gel characterized
 730 through selective dissolution and FTIR spectral subtraction," *Cem. Concr. Res.*, vol. 70, pp. 39–49, 2015,
 731 doi: 10.1016/j.cemconres.2015.01.006.
- 732 [60] N. K. Lee and H. K. Lee, "Reactivity and reaction products of alkali-activated, fly ash/slag paste,"
 733 *Constr. Build. Mater.*, vol. 81, pp. 303–312, 2015, doi: 10.1016/j.conbuildmat.2015.02.022.
- 734 [61] B. Walkley, R. San Nicolas, and S. Bernal, "Effect of MgO incorporation on the structure of synthetic
- 735 alkali-activated calcium aluminosilicate binders," Conf. 27th Bienn. Natl. Conf. Concr. Inst. Aust., no.
- August 2015, 2015, [Online]. Available:
- 737 https://www.researchgate.net/publication/303968983_Effect_of_MgO_incorporation_on_the_structure_
- 738 of_synthetic_alkali-activated_calcium_aluminosilicate_binders.

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