Characterisation of UO₂ Spent Nuclear Fuel Samples containing Gd₂O₃ using SERPENT-2 Code

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Introduction

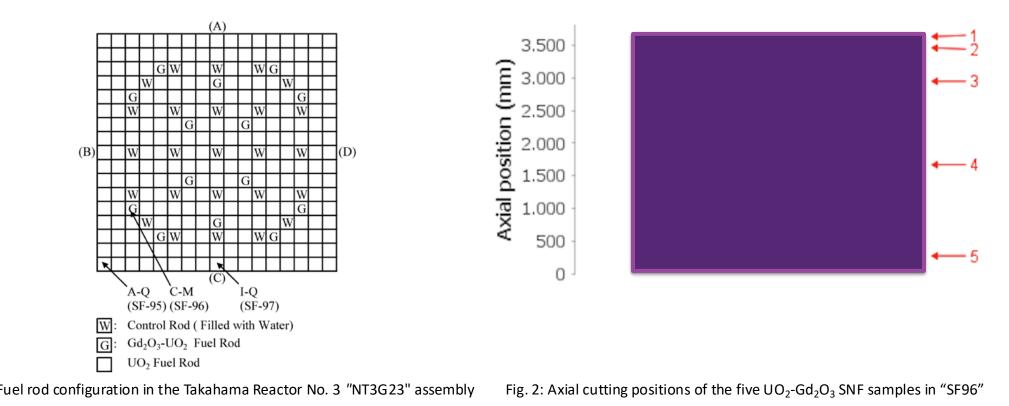
The degree of enrichment in uranium dioxide (UO₂) nuclear fuels has evolved to the extent that the associated excess reactivity at reactor start-up requires additional compensation through the addition of gadolinium(III) oxide (Gd₂O₃). However, due to the increasing presence of Gd₂O₃, the accurate prediction of the isotopic evolution and power distribution throughout the irradiation cycles has a more significant impact on the fuel performance. Nevertheless, to date there have been no studies that have evaluated the predictive capabilities of the SERPENT-2 nuclear depletion calculation code for low-doped UO₂-Gd₂O₃ fuel samples.

Method

Therefore, this master's thesis models selected UO₂-Gd₂O₃ Spent Nuclear Fuel (SNF) samples and compares them with experimental concentrations from destructive radiochemical analyses to evaluate the predictive capabilities of SERPENT-2. The simulation models incorporate SNF sample design data and reactor operating histories from the "Spent Fuel Isotopic Composition 2.0" database, which was developed by the Organisation for Economic Co-operation and Development Nuclear Energy Agency. The eight selected SNF samples were sourced from the Japanese Pressurised Water Reactors (PWRs) Takahama Reactor No. 3 and Ohi Reactor No. 2.

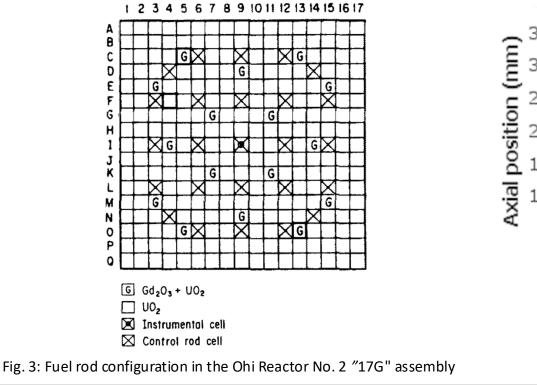
Takahama Reactor No. 3 "NT3G23" Assembly

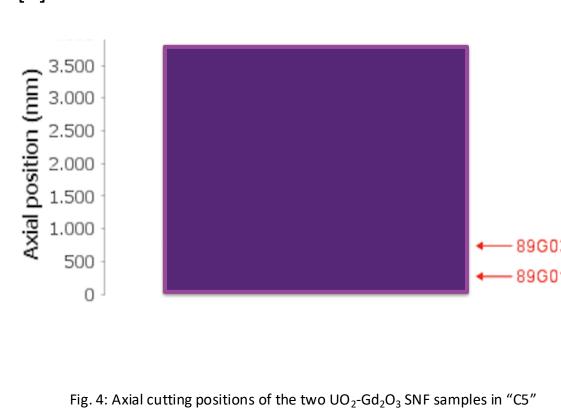
The Takahama Reactor No. 3 "NT3G23" assembly was a 17 x 17 square lattice (Fig. 1) comprising The Ohi Reactor No. 2 "17G" assembly was a 17 x 17 square lattice (Fig. 3) comprising 16 UO₂-14 UO_2 -Gd $_2O_3$ – which contain 6.00 wt% of natural gadolinium – fuel rods (e.g. "SF96") and 250 regular UO₂ fuel rods (e.g. "SF95") [1]. The five UO₂-Gd₂O₃ SNF samples, identified as "SF96-1" through "SF96-5", were positioned axially within fuel rod "SF96" (Fig. 2) and were irradiated for two consecutive cycles [2].



Ohi Reactor No. 2 "17G" Assembly

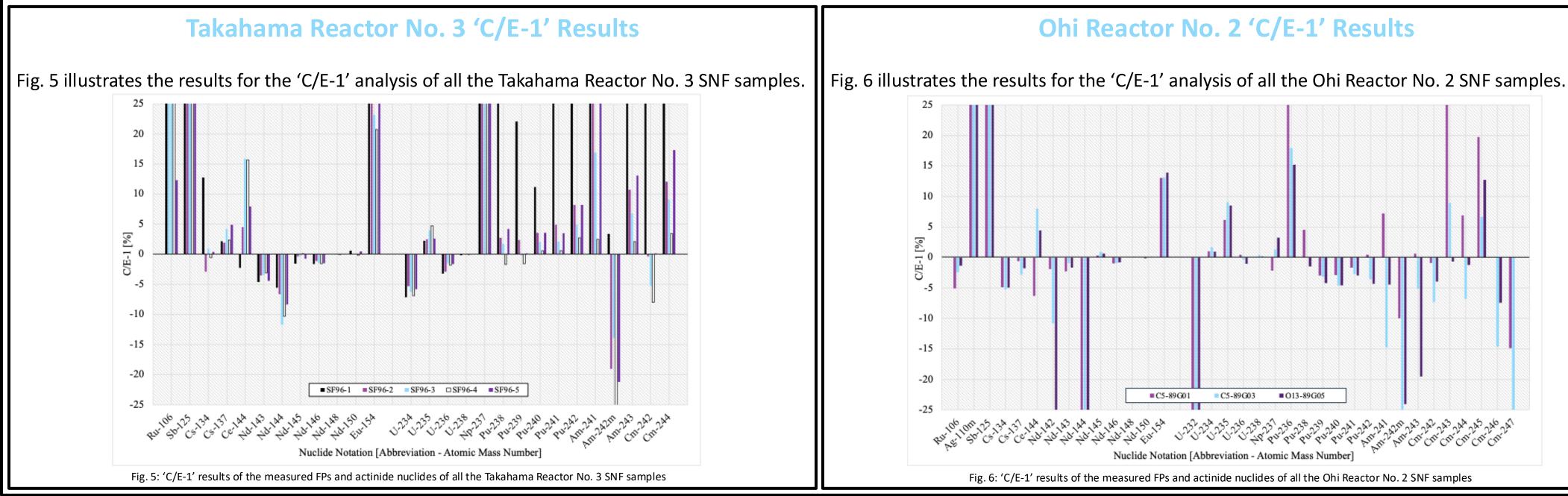
Gd₂O₃ – which contain 6.00 wt% of natural gadolinium – fuel rods (e.g. "C5" and "O13") and 248 regular UO₂ fuel rods (e.g. "F4") [3]. The three UO₂-Gd₂O₃ SNF samples, identified as "C5-89G01", "C5-89G03", and "O13-89G05", were positioned axially within fuel rods "C5" and "O13" (Fig. 4), and were irradiated for two consecutive cycles [4].

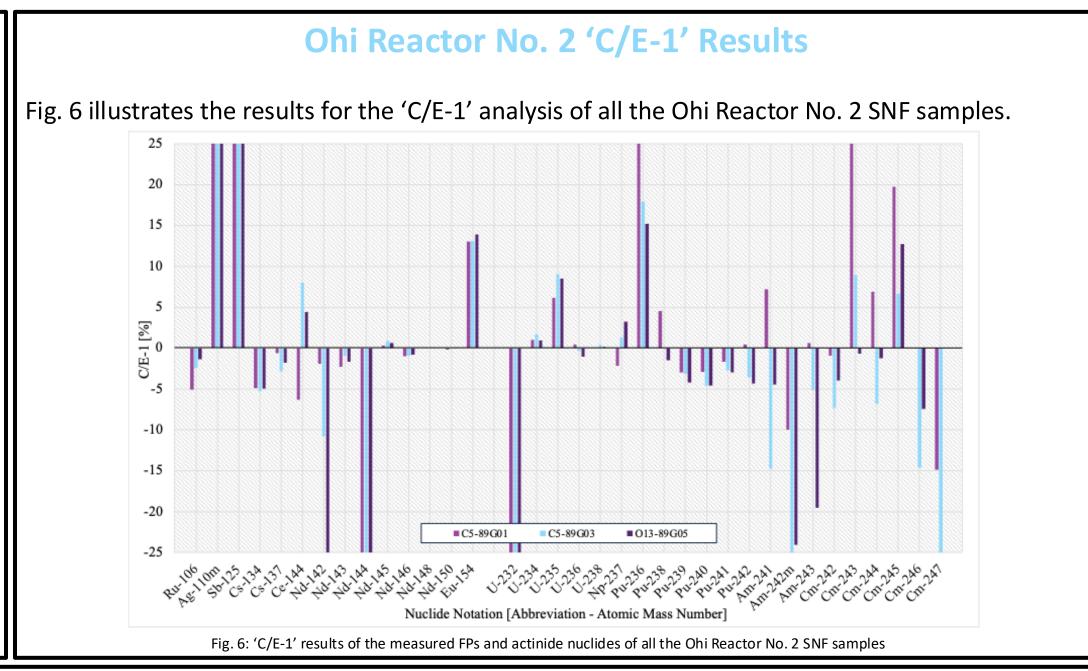




Results

Following the completion of the SERPENT-2 simulations, the nuclide inventory predictions were compared with the experimental measurements utilising the 'C/E-1' representation. The experimental measurements – performed at the 'JAERI post-irradiation fuel examination facility' – were normalised to the date at which the irradiation was concluded. The nuclear data utilised in this study were obtained from the ENDF/B-VII.1 evaluated nuclear data library.





Conclusion

For both investigated PWRs, the nuclide inventory predictions were in good agreement with the experimental results. Therefore, in the scope of validating PWR-SNF samples in which Gd_2O_3 is more prevalent, the **SERPENT-2** nuclear depletion code can be utilised.

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[1] Y. Nakahara, K. Suyama, and T. Suzaki, "Technical development on burn-up credit for spent LWR fuels," JAERI., Tokyo, Japan Tech. Rep. *JAERI-TECH--2000-071*, 2000. [2] Y. Nakahara et al., "Nuclide Composition Benchmark Data Set for Verifying Burnup Codes on Spent Light Water Reactor Fuels," *Nucl. Technol.*, vol. 137, no. 2, pp. 111-126, 2002, doi: 10.13182/NT02-2. [3] K. Suyama, M. Murazaki, K. Ohkubo, Y. Nakahara, and G. Uchiyama, "Re-evaluation of Assay Data of Spent Nuclear Fuel obtained at Japan Atomic Energy Research Institute for validation of burnup calculation code systems," Ann. Nucl. Energy, vol. 38, no. 5, pp. 930-941, May 2011, doi: 10.1016/j.anucene.2011.01.025. [4] T. Adachi et al., "Comparison of Calculated Values with Measured Values on the Amount of TRU and FP Nuclides Accumulated Gadolinium Bearing PWR Spent Fuels," JNST, vol. 31, no. 10, pp. 1119-1129, Oct. 1994, doi: 10.1080/18811248.1994.9735266.





